ENGINEERING ANALYSIS REPORT AND
INITIAL DECISION THAT THE SUBJECT VEHICLES
CONTAIN A SAFETY-RELATED DEFECT

October 17, 1994
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EXECUTIVE SUMMARY

This Engineering Analysis was opened on December 8, 1992, as a result of granting a petition from the Center for Auto Safety (CAS) and Public Citizen to "initiate a defect investigation into and recall all Chevrolet/GMC full-sized pickups (C/K-series) with fuel tank(s) . . . mounted outboard of frame rails." The objective of the investigation was to determine whether certain model year 1970-1991 Chevrolet and GMC full-sized pickup trucks contain a defect that poses an unreasonable risk to safety, related to the danger of fires following crashes, with primary focus on side-impact crashes. In the investigation, the National Highway Traffic Safety Administration’s (NHTSA) Office of Defects Investigation (ODI) conducted analyses of real-world accident data and performed laboratory crash tests of the subject and peer vehicles. ODI also addressed questions related to the compliance of these trucks with Federal Motor Vehicle Safety Standard (FMVSS) No. 301, "Fuel System Integrity." Additionally, ODI examined whether the fuel tanks and related components on the trucks were unduly affected by corrosion that could make them more likely to be involved in a fire.

On April 9, 1993, ODI sent a recall request letter to General Motors Corporation (GM), recommending that GM conduct a safety recall on GM trucks with fuel tanks mounted outside the frame rails (subject vehicles). That letter was based on two principal factors:

1. Real-world accident data in the Fatal Accident Reporting System (FARS) indicate that there is an increased risk of fatality caused by fire in side-impact crashes involving the subject vehicles compared to 1973-1987 Ford full-sized pickup trucks. That increased risk led to an estimate that, in 1993, an additional 5-6 fatalities would occur in side-impact crashes involving the subject vehicles compared to what would occur if those trucks had the same side-impact fire performance as full-sized Ford pickups.

2. Laboratory crash tests corroborated the findings from the real-world accident data analysis. That is, in certain comparable side-impact crash tests, GM fuel tanks leaked and Ford tanks did not. Further, these tests used instrumented test dummies. Dummy measurements indicate that humans could have survived the crash forces at the impact speeds at which the subject vehicles leaked. While these speeds are well in excess of the impact speed specified in FMVSS No. 301, the results indicate the increased fire risk in the GM trucks in crashes that are otherwise survivable.

GM provided an extensive amount of data and arguments in response to the recall request letter. ODI has completed an exhaustive review and analysis of the GM submissions and has conducted a variety of additional analyses associated with issues involved in this investigation. These include:

- an assessment of the effect of corrosion on fuel tank leakage and fire performance in the subject vehicles;

- an analysis of non-fatal burn injuries in side-impact crashes involving the subject vehicles;
an in-depth review of all available police accident reports and other records of side-impact, fire-involved fatal crashes involving the subject vehicles to assess the crash conditions and severity of each;

an update of the FARS analysis that led to the April 9, 1993 recall request letter;

an analysis of the reasonableness of GM's decision to design the subject vehicle with side-mounted fuel tanks, given what GM knew about the safety risks associated with that design and the availability of feasible alternative designs; and

an analysis of the information about the risk of post-crash fuel leaks that became available to GM during the time the subject vehicles were being manufactured.

**Principal Findings:**

- A review of GM submissions, as well as ODI testing, indicates that there are no data on which to conclude that the GM trucks to which FMVSS No. 301 applied, when new, did not comply with the standard.

- There are no data to indicate a relationship between fuel tank corrosion and increased fire risk in the subject vehicles, either in side impacts or in non-crash incidents.

- Apart from the basic decision to locate the fuel tanks of the subject vehicles outside of the frame rails, many of the specific features of the design of the fuel storage system and the surrounding area have increased the likelihood of post-crash fuel fires in the subject vehicles.

- Based on a review of 1979-1993 accident data reflecting the performance of full-sized pickups in side-impact fatal crashes involving fire, occupants of the subject vehicles experienced 2.8 times as many fire-related fatalities (i.e., fatalities in crashes in which a fire occurred) per million registered vehicle-years as occupants of Ford pickups and 2.5 times as many as occupants of Dodge pickups. Where the FARS code indicated that the most harmful event (MHE) of the crash was fire, the GM-to-Ford occupant fatality per million registered vehicle-years ratio is 3.4 to 1, and the GM-to-Dodge ratio is 6.1 to 1.

- Real-world accident data do not support GM's contention that GM and Ford pickup trucks have comparable side-impact fire performance and that differences in driver demographics and driver behavior explain the difference in the rates of fire-related and MHE=fire fatalities in side-impact crashes for the GM and Ford pickups. This is demonstrated by the tremendous reduction in the rate of MHE=fire side-impact fatalities that occurred after GM moved the fuel tanks for these pickups inside the frame rails in model year 1988.

- Contrary to GM's contentions, the MHE coding in FARS is a reliable indicator of the number of fatalities actually caused by fire.
• FARS data indicate that, if past trends continue, there would be approximately five additional fatalities due to fire in side-impact crashes in 1994 compared to what would occur if the subject vehicles had the same side-impact fire performance as Ford full-sized pickups.

• Reports of non-fatal burn injuries indicate that, if past trends continue, there would be three to four additional non-fatal burn injuries in 1994 in side-impact crashes involving the subject vehicles compared to the Ford pickups.

• Laboratory crash data indicate that, at certain impact speeds and configurations, the subject vehicles will leak fuel in side impacts, while comparable Ford pickups will not.

• While the crash severities in fatal side-impact, fire-involved crashes involving the subject vehicles are far in excess of the severity specified in FMVSS No. 301, they are generally less than the severities that result in fires in fatal side-impact crashes involving the Ford pickups.

• GM was aware at the time it designed the subject vehicles in the early 1970s that side-mounted fuel tank design presented an increased risk of post-crash fuel fed fires in side impacts, compared to the risk associated with other feasible alternative designs. Moreover, GM obtained additional information demonstrating the increased risk associated with the side-mounted tanks during the 15-year period the subject vehicles were in production.

**Principal Conclusions:**

• The increased risk of death and injury from fire in side-impact crashes involving the subject vehicles is a result of the design of their fuel storage system, primarily the location of the fuel tanks outside of the frame rails, supplemented by other features of the design.

• Given the state of the art at the time and GM’s awareness of the likely consequences, it was unreasonable for GM to design the subject vehicles with fuel tanks outside the frame rails.

• The increased safety risk due to post-crash fires in the subject vehicles is unreasonable.

Therefore, on the basis of the entire investigative record, I have initially decided, pursuant to 49 U.S.C. § 30118(a) (formerly section 152(a) of the National Traffic and Motor Vehicle Safety Act), that the subject vehicles contain a defect that relates to motor vehicle safety.
ENGINEERING ANALYSIS EA92-041
GM TRUCK DEFECT INVESTIGATION

A. BACKGROUND

This Engineering Analysis was opened to investigate whether General Motors (GM) 1970-1991 full-sized pickup trucks and chassis-cabs with fuel tanks located outside the frame rails (the subject vehicles) contain a "defect which relates to motor vehicle safety" within the meaning of section 152 of the National Traffic and Motor Vehicle Safety Act (the Act), recently recodified as 49 U.S.C. § 30118. Under the Act, "defect" is defined to include "any defect in performance, construction, components, or materials in motor vehicles," while "motor vehicle safety" is defined as "the performance of motor vehicles . . . in such a manner that the public is protected against unreasonable risk of accidents occurring as a result of the design, construction or performance of motor vehicles and is also protected against unreasonable risk of death or injury to persons in the event accidents do occur . . . ." The alleged defect relates to the performance of the subject vehicles in protecting against post-crash fuel leaks and fire in crashes, with primary focus on side-impact crashes.

This investigation has, from the outset, been different from the majority of safety defect investigations conducted by ODI. First, it involves a "crashworthiness" aspect of vehicle performance, while most of ODI's defect investigations involve "crash avoidance" issues; e.g., braking problems, steering problems, etc. In addition, in most investigations, the alleged defect involves a system or component that does not function the way it was designed, e.g., "a broken part." In such investigations, the alleged defect often appears in only a small percentage of the vehicles under investigation, and ODI's initial inquiry is on how many of the vehicles covered by the investigation have experienced the alleged defect. Only if the defective condition exists in more than a de minimis number of vehicles does ODI proceed to analyze whether the defect relates to motor vehicle safety.

In this case, since the alleged defect is inherent in the design of the fuel storage system of the subject vehicles, all of the subject vehicles have the alleged defect. Thus, the issue of whether the vehicles have a safety-related defect turns on the issue of whether that design creates an "unreasonable risk of death or injury to persons" in the event of a crash.

B. THE PETITION FOR A DEFECT INVESTIGATION

In a letter dated August 14, 1992, CAS and Public Citizen petitioned NHTSA to "initiate a defect investigation into and recall all Chevrolet/GMC full-sized pickups (C/K-series) with fuel tank(s) . . . mounted outboard of frame rails." The petitioners alleged that, because of the location of the tanks, "there is no frame member to protect the tank from crush in side
impact or sideswipe." The petitioners further alleged that GM concealed that it was aware of a design defect and continued to market vehicles with this design through 1987.1

Included with the petition were brief descriptions of 51 incident reports allegedly involving fuel tank fires in pickup trucks, including the subject vehicles. Of those incidents cited by the petitioners, 19 involved full-sized GM pickup trucks and/or chassis-cabs with side-mounted fuel tanks. However, based on the information provided in two of these 19 incidents, the agency cannot determine whether the side-mounted fuel tank was compromised. Eighteen involved GM vehicles outside the scope of the investigation (passenger cars, pre-1973 trucks, and heavy duty trucks). Another 13 involved non-GM vehicles. Additionally, the year/make/model of one vehicle could not be determined.

In three subsequent letters, dated September 14, October 5, and November 13, 1992, the petitioners identified additional lawsuits and provided arguments and supporting data, including the contention that the subject vehicles "do not comply with Federal Motor Vehicle Safety Standard No. 301." The petitioners also presented deposition testimony from Mr. Ronald Elwell, a former GM engineer, who testified about crash tests conducted by GM on these vehicles in the early 1980's. The petitioners alleged that, "as Mr. Elwell's depositions show, these tests clearly revealed the hazards of the side tanks outside the frame because the tanks of the test vehicles ruptured like split melons." Subsequent submissions by the petitioners concerning the investigation are also in the public file.

Upon receipt of the petition, ODI wrote a letter to GM to request information on relevant vehicle production volumes, vehicle testing, consumer complaints, accidents, fatalities, injuries, and lawsuits. The agency also sent letters to Ford Motor Company (Ford) and Chrysler Corporation (Chrysler) to obtain comparable information, such as crash test reports, complaint data, and lawsuits, about "peer" full-sized pickup trucks. In addition, ODI initiated an analysis of accident data files to assess the performance of these trucks in real-world crashes and began a series of crash tests.

Based on the petition and its supplements, manufacturer responses, real-world accident data analysis, and crash tests conducted by ODI, the petition was granted on December 8, 1992, and this engineering analysis was opened.

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1 The public file for this investigation is divided into a defect petition file (DP92-016), which contains the documents received or prepared by ODI during its consideration of the petition for a defect investigation (i.e., between August 14, 1992 and December 8, 1992), and an Engineering Analysis file (EA92-041), which contains the documents received or prepared by ODI after the petition was granted. The pages of the documents in the EA file are numbered consecutively and cumulatively in a "Bates" numbering system, and page references in this Report to such documents will be to their six-digit Bates page number. Each separate document and exhibit in the DP file has its own individual number, based on its date of receipt, but they were not given cumulative page numbers. Thus, page references in this Report to such documents will be to their DP document or exhibit number (where applicable) and to their own internal pagination.
C. **SCOPE OF THE INVESTIGATION**

- The "subject vehicles" are all model year 1973 through 1991 full-sized GM pickup trucks and cab-chassis (through the 30/3500 series) equipped with fuel tank(s) mounted outboard of the main frame rails. For model year 1970 through 1986, GM labeled the two-wheel (2wd) drive truck as a C model and the four-wheel (4wd) drive as a K model. Starting in 1987, the C and K model names were changed to the R and V model names, respectively, for vehicles equipped with fuel tanks outside the frame rails. The R and V models continued through 1991.\(^2\) GM rates the truck's carrying capacity as \(\frac{1}{2}\)-ton (Chevrolet 10 series, GMC 15 series, and Chevrolet/GMC 1500 series), \(\frac{3}{4}\)-ton (Chevrolet 20 series, GMC 25 series, and Chevrolet/GMC 2500 series), and 1-ton (Chevrolet 30 series, GMC 35 series, and Chevrolet/GMC 3500 series).

- The alleged defect is any failure, malfunction, or performance of the fuel storage system in the subject vehicles that results in, or could result in, fuel leakage and/or fire as a result of a vehicle crash.

D. **FEDERAL MOTOR VEHICLE SAFETY STANDARD NO. 301, "FUEL SYSTEM INTEGRITY**

NHTSA established FMVSS No. 301, "Fuel System Integrity," to "reduce deaths and injuries occurring from fires that result from fuel spillage during and after motor vehicle crashes" (49 CFR § 571.301). The standard addresses fuel system integrity in various crash modes, including side-impact, by limiting the amount of fuel that may leak during and after the crash test. Originally, only passenger cars had to conform with the FMVSS No. 301 requirements. However, beginning with the 1977 model year, light trucks (including the subject vehicles) had to comply with FMVSS No. 301 requirements for 30-mph frontal impacts. Trucks with a Gross Vehicle Weight Rating (GVWR) of 6,000 lbs or less also had to comply with requirements for 30-mph rear impacts. The following model year, 1978, the 20-mph side and 30-mph rear-impact requirements also became applicable to all vehicles of 10,000 lbs GVWR or less, including the subject vehicles.

E. **DEVELOPMENT OF THE FUEL TANK SYSTEM IN THE SUBJECT VEHICLES**

The fuel tanks in the subject vehicles are mounted outboard of the main frame rails, as shown in Figure 1. Prior to 1973, the standard fuel tank in GM's full-sized pickups was located inside the vehicle cab (Figure 2). Beginning in 1970, owners could have Chevrolet or GMC dealers install one or two 18.5 gallon auxiliary tanks outside of the frame rails. Also in 1971, there was a factory-installed optional auxiliary tank which could be located behind the rear axle between the frame rails. GM stated in its October 9, 1992 response to ODI's first information request (DP #12, at page 40), that this was offered to provide

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\(^2\) Since model year 1988, GM has used the C and K model designation for its newly-designed trucks with fuel tanks located inside the frame rails.
additional fuel capacity. With the 1971 model year, GM offered production option NL2, which was a GM factory-installed (as opposed to dealer-installed) 19-gallon auxiliary fuel tank located outside the driver's side frame rail.

Figure 1. Location of Fuel Tank in Subject Vehicles (Outside Frame)

Figure 2. GM Pickup Standard Fuel Tank Mounted Inside the Vehicle Cab (Model Year 1972 and Earlier)
For model year 1973, GM redesigned the entire C/K truck for the first time since model year 1963. Depending upon wheelbase and equipment chosen, these vehicles were equipped with single or dual 16- or 20-gallon fuel tanks. All vehicles came equipped with a standard tank located outside the right (passenger side) frame rail. Those purchasers choosing to increase fuel capacity could order an optional fuel tank which was mounted outside the left (driver side) frame rail. The optional tank's capacity always matched that of the standard tank, i.e., GM never offered C/K's with a 16-gallon tank on one side and a 20-gallon on the other. In the model year 1981 trucks, GM moved the standard fuel tank location from outside the right frame rail to outside the left frame rail. The optional fuel tank was then placed outside the right frame rail.

When designing the 1973 truck, GM provided enough fuel capacity to permit a range of 400 miles. At that time, GM anticipated the vehicles would average approximately 10 miles per gallon and thus made available up to 40 gallons of fuel capacity. According to GM (October 9, 1992 response (DP #12) at page 40), it did this, "to meet the needs of GM customers who had been demanding additional fuel capacity since the late 1960's."

Beginning in model year 1981 GM offered the trucks with a standard 16-gallon tank (short wheelbase) and 20-gallon tank (long wheelbase) mounted outside the left frame rail. If additional fuel capacity was desired by the purchaser, GM provided dual 16-gallon tanks for pickups rated at less than 8,600 lbs. GVWR and dual 20-gallon tanks for pickups rated at 8,600 lbs. GVWR and higher.

F. PREVIOUS INVESTIGATIONS AND RECALL

F.1. EA74-259: Fuel Tank on 1974 Chevrolet Pickups

In early 1974, ODI received a letter from the West Virginia Governor's Highway Safety Administration, regarding the puncture of a fuel tank on a 1974 pickup truck. The letter stated that the fuel tank located on the right-hand side of a 1974 Chevrolet pickup truck leaked as a result of being struck by flying debris as the truck passed another vehicle. The writer expressed concern that, although a guard was provided for most of the tank, this guard did not cover the complete tank, and alleged that the design constituted a safety hazard.

ODI found that a plastic shield was attached to the seam welded flange on the front of the tank and was bolted to a bracket mounted to the frame. ODI analyzed the complaint from the standpoint of the degree of protection that the plastic shield provided from damage caused by stones thrown up as the truck drove down a highway. At that time, ODI had no other complaints on this issue. Based on the lack of complaints and no indication of a possible defect trend, the investigation was closed on June 6, 1974.

On March 20, 1990, ODI opened an investigation concerning alleged corrosion of the fuel tanks in GM's 1984 through 1986 C/K pickup trucks. The plastic shield, which covered the bottom, front, and back of the tank, was collecting road debris, such as mud and sand, thus allowing moisture retention around the tank. It was alleged that this resulted in increased corrosion and fuel tank leakage.

No accidents, fires, lawsuits, or injuries were reported as a result of this alleged defect. ODI received 28 complaints, and GM forwarded 132 complaints during the investigation. There were no warranty claims, since the tanks usually corroded at high mileage.

During the investigation, the agency conducted a survey of vehicles in the Columbus, Ohio, area. Twelve vehicles were examined. Of those 12, 2 were found to be weeping fuel when the shield was removed, but the leak was so small that it was unmeasurable.

ODI also contracted with Calspan Corporation to have a telephone survey performed. This survey of 381 owners in six states obtained information related to fuel tank leakage. The purpose of the survey was to determine the number of owners who had experienced a problem with fuel tank leakage or noticed odors of fuel from the tank area of the vehicle. The owners were located in the states of Florida, Louisiana, Michigan, Minnesota, Missouri, and Texas. The survey found that 11.8 percent (45 out of 381) of the owners reported their vehicles had a fuel tank replaced due to corrosion. An additional 14 owners reported noticing fuel leakage, but had not replaced the tank. The average mileage of the vehicles with replaced tanks was approximately 94,700 miles and the average age was 7 years.

The investigation was closed on February 24, 1992 because the complaint rate was low, the average mileage and age of vehicles with leakage was high, and there were insufficient data to indicate the presence of a safety-related defect.


In January 1987, GM recalled 61,668 1984-1986 1-ton chassis-cab trucks to install a plastic shield over the nose of the fuel tank(s) to prevent the "sled runner" (a structural rib intended to strengthen the cab floor) from puncturing the upper right corner of the fuel tank in a crash. GM discovered this condition as a result of its crash test C-6514 conducted on April 22, 1986. In that test, a C-30 chassis-cab equipped with a low service body (similar to what utility companies use) was subjected to a 30 degree oblique frontal impact at 30 mph, consistent with the test conditions required by FMVSS No. 301. The vehicle test weight was 8,500 lbs. The test resulted in leakage when, due to vehicle crush and frame deformation, the fuel tank was punctured by the sled runner.

An earlier crash test conducted by GM (test number C-4308, October 18, 1977) had resulted in a fuel tank failure due to a sled runner-to-tank puncture in a C-30 test vehicle ballasted to an 8,500 lb. test weight. The problem was corrected at that time through the installation of a plastic shield over the leading edge of the fuel tank. The efficacy of this shield was then
confirmed during tests C-4350, C-4351, and C-4360 (conducted between December 1977 and January 1978) when no tank puncturing was observed at a vehicle test weight of 8,500 lbs. Based on GM’s engineering judgment, all 1978 through 1993 C-30 chassis-cabs were certified to comply with FMVSS No. 301 when tested at their maximum test weight of 8,500 lbs. On May 15, 1986, GM Truck and Bus Engineering reported that a possible noncompliance with FMVSS 301 existed on certain chassis-cab models. On January 15, 1987, GM notified NHTSA that it would conduct a safety recall (87V-002) to address this noncompliance.

On April 19, 1993, ODI sent an information request to GM to gather pertinent information relating to the 1987 recall and to ascertain whether it might be related to the current investigation. GM responded on May 14, 1993. In summary, GM stated that due to an engineering oversight, the sled runner shield had been omitted from the 1984-1986 C-30 chassis-cabs, thus necessitating the 1987 recall.

G. DESIGN, MATERIAL, AND/OR PRODUCTION MODIFICATIONS

Throughout the production run of the subject vehicles, GM made a number of changes to the design of the fuel system. A detailed description of these design changes is contained in the public file for this investigation. The following summarizes the most significant changes.

- Model year 1975—the filler neck was changed to meet evaporative emission requirements. The new filler neck had a built-in trap door nozzle restrictor to prevent the use of service station nozzles that dispense leaded gasoline. Also, the fuel system was sealed and vented to a charcoal canister.

- Model year 1978—a flange was added to both lower rear corners of the cab to improve fuel system integrity in side impacts.

- Model year 1979—the filler cap and filler neck were recessed behind a body panel door.

- Model year 1980—a “radius” was added to both lower rear corners of the cab to improve fuel system integrity in side impacts.

- Model year 1981—the standard fuel tank location was changed from the right side to the left side, and the optional tank location was changed from the left side to the right side.

- Model year 1984—the tank supports were modified, a new plastic shield was added to improve performance in side impacts, and a new filler neck support housing was added.
H. COMPLAINTS

ODI has received and analyzed reports from a variety of sources (including GM) concerning fuel tank failures that occurred due to impact and/or corrosion. Where possible, ODI has attempted to compare complaints received from these sources with the data contained in NHTSA's Fatal Accident Reporting System (FARS) (a census of fatal crashes from 1975 forward). In some cases, reconciliation is not possible due to the nature of the information, e.g., the accident did not involve fatalities, or occurred so recently that it has not yet been entered into FARS. The information in this section is current through April 1, 1994.

ODI has reviewed information about 555 accidents that appear to be relevant to this investigation; i.e., the report involves at least one C/K truck with fuel tanks located outside the frame rails, and fuel leaked from the C/K’s fuel tank(s). In addition, ODI has also received complaints of fuel tank corrosion. However, none of these allege a vehicle fire. The corrosion reports are discussed in detail in section M.1.

Table 1 shows the number of reported incidents involving the alleged defect from January 1973 through April 1994 that have been received from all sources, with duplicate reports removed.

<table>
<thead>
<tr>
<th></th>
<th>GM</th>
<th>Other Sources</th>
<th>TOTAL</th>
</tr>
</thead>
<tbody>
<tr>
<td>Accidents with Fuel Leak</td>
<td>525</td>
<td>30</td>
<td>555</td>
</tr>
<tr>
<td>Fuel Leak, Fire</td>
<td>480</td>
<td>30</td>
<td>510</td>
</tr>
<tr>
<td>Fuel Leak, No Fire</td>
<td>30</td>
<td>0</td>
<td>30</td>
</tr>
<tr>
<td>Fuel Leak, Fire Unknown</td>
<td>15</td>
<td>0</td>
<td>15</td>
</tr>
<tr>
<td>Non-Fatal Burn Injuries (Accidents/Injuries)</td>
<td>103/156</td>
<td>2/2</td>
<td>105/158</td>
</tr>
<tr>
<td>To Truck Occupants (Accidents/Injuries)</td>
<td>86/127</td>
<td>2/2</td>
<td>88/129</td>
</tr>
<tr>
<td>To Striking Vehicle Occupants (Accidents/Injuries)</td>
<td>17/29</td>
<td>0/0</td>
<td>17/29</td>
</tr>
</tbody>
</table>

In addition to the complaints reflected in the above table, ODI has reviewed FARS data reflecting a total of 284 fire-involved, side-impact fatal crashes involving a subject vehicle that occurred during the period 1975-1993. Those 284 crashes resulted in 341 fatalities to occupants of the subject vehicles and 29 fatalities to occupants of the striking vehicle, for a total of 370 fire-related fatalities.
I. SUBJECT VEHICLE POPULATION

GM produced 9,219,248 of the subject vehicles from model year 1973 through 1991. GM was unable to state how many 1970 through 1972 trucks were equipped with the optional auxiliary tank located outside of the frame rail(s). Additionally GM was unable to state how many of the 1973 through 1979 trucks were equipped with dual fuel tanks, but did provide dual tank populations for 1983 through 1991 model years. Beginning with model year 1988, the standard tank location was inside of the frame rails for all pickups except for certain ¾ and 1-ton chassis-cab trucks, which retained the prior design with the tank location outside of the frame rails. Table 2 shows the number of subject vehicles produced from model year 1973 through 1991. The vast majority of subject vehicles (9,148,686) were produced from model year 1973 through 1987.

<table>
<thead>
<tr>
<th>Model Year</th>
<th>Production</th>
</tr>
</thead>
<tbody>
<tr>
<td>1973</td>
<td>743,068</td>
</tr>
<tr>
<td>1974</td>
<td>737,448</td>
</tr>
<tr>
<td>1975</td>
<td>575,684</td>
</tr>
<tr>
<td>1976</td>
<td>792,734</td>
</tr>
<tr>
<td>1977</td>
<td>914,784</td>
</tr>
<tr>
<td>1978</td>
<td>928,954</td>
</tr>
<tr>
<td>1979</td>
<td>899,592</td>
</tr>
<tr>
<td>1980</td>
<td>478,932</td>
</tr>
<tr>
<td>1981</td>
<td>487,165</td>
</tr>
<tr>
<td>1982</td>
<td>416,196</td>
</tr>
<tr>
<td>1983</td>
<td>380,199</td>
</tr>
<tr>
<td>1984</td>
<td>488,782</td>
</tr>
<tr>
<td>1985</td>
<td>513,280</td>
</tr>
<tr>
<td>1986</td>
<td>478,468</td>
</tr>
<tr>
<td>1987</td>
<td>308,400</td>
</tr>
<tr>
<td>1988</td>
<td>30,533</td>
</tr>
<tr>
<td>1989</td>
<td>24,212</td>
</tr>
<tr>
<td>1990</td>
<td>7,325</td>
</tr>
<tr>
<td>1991</td>
<td>8,492</td>
</tr>
<tr>
<td>TOTAL</td>
<td>9,219,248</td>
</tr>
</tbody>
</table>
Based on vehicle registration data obtained from the R.L. Polk Company (R.L. Polk), ODI estimates that as of July 1, 1994, 4.8 million of the subject vehicles were in use on U.S. highways.

**J. SERVICE BULLETINS:** GM issued no service bulletins related to the alleged defect.

**K. COMPLIANCE WITH FMVSS NO. 301**

As noted in section B, the petitioners claimed that the subject vehicles "do not comply with Federal Motor Vehicle Safety Standard No. 301." To address the compliance issue, ODI requested GM's certification data to assess its basis for certifying compliance with FMVSS No. 301. In addition, ODI conducted a series of side-impact tests under the procedures specified in FMVSS No. 301 to further assess this issue. As noted in section D, FMVSS No. 301 specifies limits of fuel leakage from vehicles when tested in frontal, side and rear barrier impacts. For side impacts, FMVSS No. 301 requires that the vehicle be impacted laterally on either side by a flat-faced barrier moving at 20 mph. In side impacts, the barrier face is parallel to the longitudinal axis of the vehicle. The barrier is 24 3/4 inches high, 78 inches wide, has a ground clearance of 5 inches, and weighs 4,000 lbs. The vehicle's fuel tank is filled to between 90 and 95 percent of capacity with stoddard solvent, a liquid that has similar characteristics to gasoline, but is much less flammable. In accordance with FMVSS No. 301, two uninstrumented test dummies are positioned in the outboard seating positions for these tests. Fuel spillage may not exceed 1 ounce by weight from impact until motion of the vehicle has ceased, and shall not exceed a total of 5 ounces by weight in the 5-minute period following cessation of motion. For the subsequent 25-minute period following cessation of motion, fuel spillage during any 1-minute interval may not exceed 1 ounce by weight.

The majority of C/K trucks covered by this investigation were required, when new, to comply with the requirements of FMVSS No. 301.

**K.1. Legal Issues**

GM has contended that because the subject vehicles comply with FMVSS No. 301, and because safety standards must "meet the need for motor vehicle safety," NHTSA lacks the authority to determine that they contain a safety-related defect. NHTSA disagrees.

Under the Safety Act, all vehicles, when new, must comply with all applicable Federal motor vehicle safety standards. The Act defines motor vehicle safety standards as "minimum standards for motor vehicle performance . . ." (emphasis supplied). Moreover, NHTSA's concerns are not limited to whether a product complies with safety standards when new, but also include whether it protects the driving public against an unreasonable risk of accidents, injuries, and death throughout its lifetime. The provisions of Part B of the Act, authorizing recalls to correct safety defects as well as noncompliances, supplement and complement the statutory provisions for adoption and enforcement of safety standards to maximize the protection of the public.
Under 49 U.S.C. § 30111 (formerly section 103 of the Safety Act, NHTSA’s safety standards must be "practicable," "meet the need for motor vehicle safety," and be stated in "objective terms." They must also be "reasonable, practicable, and appropriate for the particular type of motor vehicle" for which they are prescribed.

It is impossible to promulgate standards that will ensure that all designs and manufacturing processes do not create unreasonable safety risks. Nor can standards for new vehicles completely guard against designs or processes which, over time, lead to unreasonable risks to the driving public, because of factors such as manufacturing flaws, deterioration, or the manner in which vehicles are operated. It is also impossible to ensure that laboratory tests adequately represent all real-world crash circumstances. Thus, even if a vehicle’s fuel system did not leak under the specific test conditions set out in FMVSS No. 301, it might still present an unreasonable safety risk under different real-world crash conditions. If a particular aspect of a vehicle’s design or performance appears to create an unusually high risk of accidents, deaths, or injuries, it is appropriate for the agency to investigate whether the vehicle contains a safety defect.

K.2. GM Certification Testing

GM provided information detailing the basis for its certification that these vehicles complied with the applicable requirements of FMVSS No. 301 in its responses of October 9, 1992, January 29, 1993, and April 30, 1993. In summary, the GM information indicated the following. Since FMVSS No. 301 side-impact requirements were not applicable to light trucks prior to model year 1978, no side-impact certification testing was performed for earlier model years. For the 1978 model year, GM conducted four right side and three left side tests. For model year 1979, GM conducted six tests, all to the right side, stating "the fuel tank installations are symmetrical side to side. Thus, a successful test on one side would indicate compliance of the fuel tank of the other side of the vehicle." However, GM conducted a seventh test (C-4421), the vehicle sustained 7.6 ounces of fuel leakage in the first five minutes following the side impact. Although GM certified compliance on the basis of the six passing tests, the seventh test led GM to develop a design change to "increase the margin of compliance with the side-impact requirements of FMVSS No. 301" for vehicles manufactured late in calendar year 1979 (for model year 1980) and afterward. For model year 1980, one side-impact test was performed on the right side with no fuel leaks. For model year 1981, GM performed one right and two left-side tests with no leaks. For model year 1982, there was one left-side test, with no leak. One left side test was conducted for each of model years 1983 and 1984 with no leakage noted. No side tests were performed for model year 1985 through 1990 trucks. GM stated that there were no changes made which would affect compliance with the standard. A thorough description of GM's compliance

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3 In anticipation of the effectiveness of FMVSS No. 301, in October 1975, GM conducted a side-impact test pursuant to the procedures of the standard on a 1975 C pickup truck that resulted in a leak (Test C-3701). In response to that test, and other analysis, GM modified the design of the subject vehicles to add a flange to the lower rear corners of the cab prior to the effective date of the side-impact portion of the standard.
testing and test results is contained in GM's October 9, 1992 response (DP #12 at 17-28). A summary is contained in Appendix I-D to GM's April 30, 1993 letter.

K.3. ODI Testing Pursuant to FMVSS No. 301 Procedures

Five subject and two peer vehicles were tested for ODI by the Vehicle Research and Test Center (VRTC) in East Liberty, Ohio, in accordance with the side-impact test procedures set out in FMVSS No. 301. These tests were conducted on vehicles up to 11 years old in an effort to assess performance in FMVSS No. 301 test conditions. Six vehicles (four subject and two peer) were tested with "as received" fuel tanks. A new fuel tank was installed in one other GM vehicle (a 1985 model) for testing. The tests were conducted at 20 mph with the test conditions specified in the standard, except that no static rollover subsequent to impact was performed on the first two vehicle tests. Rollovers were performed on the remaining five test vehicles. ODI's "Crash Test Protocol" for the FMVSS No. 301-type tests appears at EA 009040. The results of the testing program are described in a VRTC report, "Summary of the Crash Test Program Concerning Fuel Tank Integrity of Full-size Pickup Trucks," June 1993 (EA 005812).

Two of the four "as received" GM vehicles and the one GM vehicle tested with a new tank satisfied the side-impact fuel leakage requirements of FMVSS No. 301. The third "as received" GM truck leaked stoddard solvent from the engine compartment during the post-crash rollover. The fourth "as received" vehicle, a 1982 truck, sustained a fuel tank leak from underneath the forward tank strap. Further examination indicated that the leak resulted from fuel tank corrosion.

Based on the results of these five side-impact "compliance" tests on vehicles up to 11 years old, as well as the 20 "certification tests" submitted by GM, there are no data on which to conclude that the subject vehicles to which the standard applied, when new, did not comply with FMVSS No. 301.

L. ADDITIONAL TESTING

L.1. GM Crash Testing

GM conducted several series of fuel system integrity crash tests in addition to those related to FMVSS No. 301 compliance certification. These consisted of side-impact tests conducted at speeds greater than 20 mph with either a flat-faced barrier or a vehicle as the striking device. GM conducted 32 of these side-impact tests between January 4, 1972, and July 3, 1991. Four tests were flat-faced barrier impacts into the subject vehicle at 30 mph. These tests resulted in two fuel tank leaks. One test was a car impact into a truck at 35 mph, which resulted in a fuel tank leak. Four tests were done in support of litigation at speeds

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4 This figure does not include an unspecified number of tests conducted by or for GM in connection with litigation that have not been produced to NHTSA because GM asserts that they are protected from disclosure under the "work-product" doctrine.
ranging from 49 to 67 mph; two produced fuel tank leaks and in two, the test reports provided insufficient information to determine if a fuel leak occurred.

Beginning on July 24, 1981, GM conducted “fuel system integrity car-to-truck development corporate product performance objective (CPPO) tests” of the subject vehicles to “enhance the ability of the fuel storage system to manage significantly greater levels of energy” (GM’s October 9, 1992 response (DP #12) at page 15). Twenty-two vehicle-to-vehicle side-impact tests were conducted at speeds up to 50 mph. Three of these tests were conducted at 30 mph, and the final nineteen at 50 mph. A detailed review of GM’s CPPO testing is presented in the public file.

These tests continued through early 1984. On the basis of this test program, GM modified the fuel system for the model year 1984 to “enhance” the vehicles’ crash performance. Among other changes, the new design included a plastic shield, new lower mounting brackets with increased load-capacity, a “breakaway” filler neck, and revised welding of the tank seams.

Fluid loss was noted in all 22 CPPO tests, although not all leaks were from compromised fuel tanks. A fuel tank leak was observed in one 30-mph impact test and thirteen 50-mph tests. Fuel tank seam failures were noted in nine of those tests, tears and punctures were observed in 4 tests, and a sending unit failure accounted for one fuel tank leak. Leaks from both the fuel tank and other sources (e.g., filler pipes, vent tubes, and gas caps) were observed in five of the 50-mph tests. Eight tests resulted in fluid leaks from other sources alone. Of those, one was observed after a 30-mph impact and the other seven resulted from 50-mph impacts.

L.2. ODI Testing

ODI developed a test program to examine the crash severities at which fuel leakage occurs in the subject vehicles and in peer vehicles and the risk of occupant impact injury, based on dummy injury measurements, at such severities. Eighteen vehicle tests were conducted at VRTC in addition to the FMVSS No. 301-type tests. The test vehicles included the subject GM full-sized pickup trucks and peer vehicles. Vehicles were tested either with new fuel tank systems or in the “as received” condition. Most of the tests of the GM trucks were performed on 1986-1987 models. Some static and dynamic component tests were also performed on the subject vehicles’ fuel tanks and related parts to support the crash testing. Aside from the FMVSS No. 301-type tests described in section K.3, VRTC also conducted FMVSS No. 214-type side-impact tests, vehicle-to-vehicle side-impact tests, and pole barrier side-impact tests.

VRTC also conducted testing of three fuel tanks using the procedure specified for commercial vehicles over 10,000 lbs. in a standard issued by the Federal Highway Administration (49 CFR Ch. III, Subpart E - Fuel Systems). The purpose was to compare the performance of side-mounted tanks used on the subject vehicles with side-mounted commercial vehicle-type tanks used on certain Ford F-350 pickup trucks. The tests were conducted by filling the tanks with water to a weight equivalent to the maximum fuel load
and dropping the tank onto a hard surface from a height of 30 feet; i.e., an impact speed of approximately 30 mph. The standard allows a leakage rate not to exceed one ounce per minute by weight. Tests were performed on two GM tanks and one Ford tank. Both of the GM fuel tanks leaked most of their contents upon impact. The Ford tank leakage rate was measured to be about 11 ounces per minute by weight. All three of the tested tanks exceeded the maximum allowable leakage requirement in 49 CFR § 393.67(e)(1). The VRTC report, "Fuel Tank Drop Tests," is included in the public file for this investigation.

The principal results of the VRTC testing were as follows:

1. The single fuel tank leak (about 10 ounces/min) noted during the FMVSS No. 301-type side-impact tests was on a 1982 Chevrolet K-20, which sustained a cut in a rusty area of the tank. The other four GM vehicles tested did not leak at impact, although non-tank components of one GM and one Ford truck leaked during the post-crash rollover test.

2. No significant leaks were noted on three GM vehicles with new fuel tanks installed that were tested with the FMVSS No. 214 moving deformable barrier. In two tests (at 33 and 45 mph), the barrier was in the "crabbed" condition simulating both vehicles moving, as prescribed in FMVSS No. 214. In one test (at 45 mph), the 214 barrier was not "crabbed," but impacted the GM truck at 30 degrees from the perpendicular, with the vehicle's longitudinal axis in line with its velocity vector.

3. When impacted at the fuel tank location at a 30 degree angle from the perpendicular by a 1987 Ford Taurus at 45 mph, leaks in the GM tank were noted from the fuel gauge sending unit seal, the filler hose (which separated from the filler neck), and a small cut and a hole in a rusty area of the tank. These leak sites were verified after the tank was removed from the vehicle following the test. After subsequently refilling the tank to the sending unit O-ring, about 29 ounces leaked from the small cut before stopping after 10 minutes. An identical test with a 1987 Taurus striking a Ford pickup truck at the same impact point produced leakage of 55 ounces in one minute from the fuel reservoir mounted on the inside of the left frame rail.

4. When impacted at the fuel tank location at a 30 degree angle from the perpendicular by a 1986 GM pickup truck at 45 mph, no leakage was noted in either the GM or Ford trucks.

5. When impacted at the fuel tank location at a 30 degree angle from the perpendicular by a 1991 Chevrolet Caprice at 60 mph, leakage from the fuel tanks was noted on both the GM (tank split at one end and sprayed fluid) and Ford (small hole punched in tank) trucks.

6. When impacted at the fuel tank location at a 30 degree angle from the perpendicular by a 1991 Chevrolet Caprice at 50 mph, significant leaks/spray were noted from the tank (in "as received" and new conditions) on three GM trucks, but no leaks were
noted during a similar test on a Ford truck. Dummy injury measurements indicated that these crashes were survivable.

7. When impacted at the fuel tank location in a vehicle-to-pole test at 20 mph, leaks from the GM tank were noted from the deformed sending unit of the tank, while no leaks were noted during a similar test on a Ford. Dummy injury measurements indicated that these crashes were survivable.

8. The results of the crash test program are consistent with real-world crash data described in section N.1. That is, real-world crash data indicate a difference between GM and Ford pickups in the likelihood of fire occurrence in fatal side crashes. These tests indicate a difference in fuel tank integrity between these two vehicles in high-speed side crashes, in which dummy injury measurements indicated that these crashes were survivable.

L.3. GM Comparative Crash Testing of Ford and GM Trucks

In an effort to rebut ODI’s testing, which demonstrated that the subject vehicles are more likely to leak fuel in certain side impacts than similar Ford pickups, GM contracted with Failure Analysis Associates (FaAA) to conduct a series of rear-impact tests of full-sized Ford and GM pickup trucks to compare their fuel system integrity performance in rear crashes. Since some 1973-1987 Ford F-series trucks had optional fuel tanks mounted behind the rear axle, the FaAA testing was designed to demonstrate that vehicles with fuel tanks mounted in the rear will experience leaks in rear-impact crashes at crash severities that would not produce a leak in the subject vehicles with fuel tanks mounted on the side.

FaAA conducted two rigid pole rear-impact tests at 20 and 30 mph, and one 50-mph vehicle-to-vehicle rear-impact test on Ford pickups and a 30-mph pole rear-impact test and a 50-mph vehicle-to-vehicle rear-impact test on GM pickups. In all three tests of the Ford trucks, there was a loss of fuel system integrity. In neither of the tests of the GM trucks was there a loss of fuel system integrity.

NHTSA agrees with GM that various laboratory test conditions can be chosen that show differences in fuel system performance between two different vehicles in a particular crash mode. However, as described below, NHTSA’s finding of an increased risk of post-crash fires in the subject vehicles is based primarily on extensive analyses of real-world crashes. In real-world, side-impact fatal crashes, there is a difference between GM and Ford pickup truck fire performance. The ODI laboratory crash test results are consistent with, and support, this finding. However, FARS data indicates that in fatal, rear-impact crashes where fire caused the fatality, the GM and Ford trucks have almost identical fire performance; i.e., 0.09 fatalities per million registered vehicle-years for the Ford pickups and 0.08 fatalities per million registered vehicle-years for the subject vehicles. The objective of ODI’s crash testing was to understand the vehicle design factors which may explain real-world differences. Since available data do not suggest any real-world differences between the GM and Ford trucks in rear crashes, the GM rear-impact tests do not undercut the agency’s initial determination.
M. ADDITIONAL INFORMATION

M.1. Corrosion

As part of this investigation, ODI examined whether there was any increased risk of fire associated with corroded fuel tanks in the subject vehicles. The results of the corrosion analysis are described in the ODI report, "Corrosion and Fuel Tank Integrity," which appears in the public file for this investigation.

ODI reviewed all previous fuel tank corrosion investigations/recalls, analyzed consumer complaints received by ODI and by GM, examined FARS data to analyze the possible effects of vehicle age on fire-involved crash rates, reviewed state accident data files, analyzed State Farm Mutual Insurance Company vehicle fire claim data, analyzed vehicle fire data reported in the National Fire Incident Reporting System (NFIRS), and reviewed both original equipment manufacturer (OEM) and aftermarket fuel tank part sales.

The complaint data reflect a relatively low complaint rate regarding fuel tank leakage associated with corrosion in the subject vehicles and present no information to suggest the likelihood of fire resulting from such corrosion. Neither the FARS data nor the Michigan state accident data suggest that fuel tank corrosion in the subject vehicles contributes to fires in crashes. Similarly, the Florida state accident data do not suggest a fire problem in these vehicles due to corrosion in a non-crash environment. Insurance claims data revealed no significant difference in the fire claim rate between GM and Ford pickup trucks. The NFIRS information did not suggest that corrosion led to increased fire risk in the subject vehicles. The OEM and aftermarket parts sales information did not suggest a safety concern related to corrosion. After examining all available data from these sources, ODI has not identified any relationship between fuel tank corrosion and increased fire risk in the subject vehicles, in either side impacts or non-crash incidents.

M.2. Structural Integrity of the Subject Vehicles in a Side Impact

In its July 19, 1993, response to ODI’s June 17, 1993, information request, GM asserted that "1973-1987 C/K pickup trucks 'manage collision energies very well in side impacts' both in terms of occupant protection and fuel system integrity." GM contended that the frame rail is designed to deform in side-impact crashes in a predetermined manner to effectively manage side impact collision energies and to protect the fuel tank from rupture.

ODI agrees that the structure of the subject vehicles will deform to some extent in certain side-impact crashes, and that such deformation can help to provide protection against tank rupture in some crashes. However, as the frame and structure of the truck deform and absorb energy, the force levels transmitted through the fuel tank will increase. Thus, while the truck structure can help to provide protection against tank failure up to some level of crash severity, in severe side-impact crashes, the force being applied to the tank, and the energy absorbed by the tank, will exceed the strength of the tank material, resulting in tank failure and the loss of fuel. This is demonstrated by GM's CPPO tests, ODI's crash tests, and real-world crashes.
M.3. Ignitability of Expelled Fuel

ODI contracted with the Building and Fire Research Laboratory (BFRL) of the National Institute of Standards and Technology (NIST) (formerly known as the Center for Fire Research, National Bureau of Standards) to analyze the ignitability of fuel expelled from the subject vehicles under two different leakage scenarios. The results of this analysis are presented in the public file.

M.4. Analysis of Specific Failure Modes

This investigation has primarily focussed on the issue of whether there have been a disproportionate number of fires arising from side-impact crashes in the subject vehicles, and on an assessment of the severity of crashes that led to such fires, rather than the particular failure modes that led to such fires.

On March 24, 1994, Arndt and Associates submitted a report titled “Failure Modes of General Motors C/K Light Truck Outboard Frame, Side Mounted Fuel Containment System” (EA 054978). The Arndt report discusses numerous distinct failure modes that have led to fuel system leaks in crash tests and to fires in real-world crashes involving the subject vehicles. The report divides these failure modes into those associated with (1) tank position/mounting; (2) puncture by sharp objects surrounding the tank; (3) filler neck/cap failures; and (4) post-1983 fuel tank shield deficiencies.

Within each of these broad areas, the report notes a variety of specific failure modes. It also includes appendices, which contain photographs of parts and systems, applicable GM design documents, and references to GM and NHTSA crash tests and real-world crashes that exemplify each of the identified failure modes. In general, the report provides evidence that, even apart from the basic decision to locate the fuel tanks of the subject vehicles outside of the frame rails, many of the specific features of the GM design have increased the likelihood of post-crash fuel fires.

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5 One of the major activities of Arndt and Associates is providing consulting services to plaintiffs in products liability litigation. The report in question was commissioned by the attorneys representing the plaintiffs in a class action filed against GM in connection with claims about the fuel system integrity of the subject vehicles.

6 For example, section III of the report identifies the following "sharp objects surrounding the fuel tank:" fuel tank mounting bolt; fuel tank support strap; three different bolts/screws protruding through the cab floor; the forward leaf spring mount; fuel line mounting bolts on the right frame rail, post-1983 outboard fuel tank support; post-1983 shield mounting brackets; and the inner edge of the aft truck cab/forward edge of truck bed.
N. SAFETY RISK ANALYSIS

ODI conducted extensive analyses of real-world accidents and crash data to assess the safety risk associated with the alleged defect. The data on which these analyses were based included data collected under the agency's FARS, Police Accident Reports (PARs), autopsy reports, state accident data, insurance company data, reports of burn injuries, and crash test reports.

N.1. FARS Data

ODI's initial analysis of FARS data in this investigation is set forth in a report prepared by Susan Partyka. Fatalities, Fire-Related Fatalities, and Fatal Burns in Crashes Involving Certain Full-Sized American Pickup Trucks, NHTSA, April 26, 1993 (EA 003201). This analysis was recently updated by Ms. Partyka to include data through 1993. Fatalities, Fire-Related Fatalities, and Fatal Burns in Crashes Involving Certain Full-Sized American Pickup Trucks that Occurred from 1975 to 1993, NHTSA, June 30, 1994 (EA 058122). Both reports present comparative data on the frequency of fatalities, fire-related fatalities (i.e., fatalities in vehicles in which a fire occurred in a crash), and fatal burns (fatalities in crashes for which FARS indicates that the "most harmful event" (MHE) was fire) — both for pickup truck occupants in fatal crashes and for occupants of vehicles involved with pickup trucks in vehicle-to-vehicle fatal crashes. Considering fatal crashes in which there was a fire, the analysis uses the parameters of occupant fatalities, driver fatalities, and fatal crashes per million registered vehicle-years to assess safety performance. In addition to comparing these rates among domestic full-sized pickup trucks for all crashes, the analysis considers the rates for each individual crash mode (i.e., frontal, side, rear, and roll-over).

The focus of ODI's investigation was on side crashes in which the side-mounted fuel tank in the subject vehicles is subjected to crash forces which could result in a fuel leak and resultant fire. Although the location and mounting of the tanks also makes them vulnerable to impacts from other directions (such as sideswipes), the agency believes that this focus was appropriate, given the allegations that the tank is particularly vulnerable to side impacts.

The updated 1994 Partyka report indicates that, in calendar years 1979-1993, for all crash modes, the occupant fatality rates were 168.71 fatalities per million registered vehicle-years for the subject vehicles, 139.03 for Ford full-sized pickups, and 130.01 for Dodge full-sized pickups. As shown in Figure 3, the subject vehicles had a fatality rate per million registered vehicle-years of 30.62 in side crashes, compared to the Ford rate of 26.32, and the Dodge rate of 26.05. Further, in fatal side-impact crashes involving fire, the rate of fire-related

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7 Police Accident Reports are official reports filed by city, county, and state police officers to establish records of motor vehicle accidents. Reports generally contain information describing the vehicles involved, occupants, witnesses, vehicle speed, impact angle, road conditions, etc. The retention period varies among states, but is generally no longer than four years.
fatalities per million registered vehicle-years was 2.84 for GM, 1.03 for Ford, and 1.13 for Dodge. The ratio of the side-impact fire-related fatality rate for the GM pickup trucks to that of the Ford pickup trucks is 2.8 to 1. Finally, in those side-impact crashes in which fire was the MHE, comparative fatality rates were 1.40 for GM trucks, 0.41 for Ford trucks, and 0.23 for Dodge trucks. The difference in the side-impact MHE=fire occupant fatality rates between the GM and Ford trucks is 0.99 (1.40 - 0.41) occupant fatalities per million

Figure 3. Side-Impact Occupant Fatalities per Million Registered Vehicle-Years
registered vehicle-years. The ratio of GM to Ford rates for side-impact MHE=fire occupant fatalities is 3.4 to 1.\footnote{The GM-to-Ford comparisons set out in the updated report, using data through 1993, are essentially similar to those set out in Ms. Partyka’s initial analysis, which was based on data through 1990. For example, see Table 3 below.}

In addition to fatalities to occupants of pickup trucks involved in side impacts, the updated Partyka report also analyzed fatalities to occupants of the impacting vehicles. This analysis (Appendix A6, page 26) indicates that impacts into the side of the GM pickups resulted in an additional 0.07 occupant fatalities due to fire per million registered vehicle-years in the striking vehicle compared to what occurred in impacts into the side of Ford pickups.

Summing these two incremental increases reveals that there have been approximately 1.06 additional occupant fatalities per million registered vehicle-years involving side-impact MHE=fire crashes into the subject vehicles compared to fatalities in such crashes into Ford full-sized pickups. Given the number of subject vehicles on the road (4.8 million) as of July 1, 1994,\footnote{Because July 1 is the midpoint of the calendar year, the number of vehicles on the road on July 1 can be considered as the average number of vehicles on the road throughout the year.} NHTSA estimates that, if past trends continue, the increased risk of fire in side crashes involving the subject vehicles will result in approximately five additional fatalities in side-impact crashes in 1994.

The annual number of incremental fatalities will decrease over time as the subject vehicle population decreases. Table 4 presents these estimates through the year 2012, using the incremental rate of 1.06 occupant fatalities per million registered vehicle-years derived in the updated Partyka report.

<table>
<thead>
<tr>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>GM</td>
<td>1.47</td>
<td>1.40</td>
</tr>
<tr>
<td>Ford</td>
<td>0.42</td>
<td>0.41</td>
</tr>
<tr>
<td>GM-to-Ford difference</td>
<td>1.05</td>
<td>0.99</td>
</tr>
<tr>
<td>GM-to-Ford ratio</td>
<td>3.5 to 1</td>
<td>3.4 to 1</td>
</tr>
</tbody>
</table>
### Table 4. 1973 through 1991 GM C/K, R/V Estimated Remaining Registered Vehicles and Additional Burn Fatalities

<table>
<thead>
<tr>
<th>Year</th>
<th>Estimated Population</th>
<th>Annual Additional Burn Fatalities&lt;sup&gt;1&lt;/sup&gt;</th>
<th>Cumulative Additional Burn Fatalities&lt;sup&gt;2&lt;/sup&gt;</th>
</tr>
</thead>
<tbody>
<tr>
<td>1994</td>
<td>4,827,465</td>
<td>5.12</td>
<td>5</td>
</tr>
<tr>
<td>1995</td>
<td>4,311,760</td>
<td>4.57</td>
<td>10</td>
</tr>
<tr>
<td>1996</td>
<td>3,794,057</td>
<td>4.02</td>
<td>14</td>
</tr>
<tr>
<td>1997</td>
<td>3,288,473</td>
<td>3.49</td>
<td>17</td>
</tr>
<tr>
<td>1998</td>
<td>2,815,392</td>
<td>2.98</td>
<td>20</td>
</tr>
<tr>
<td>1999</td>
<td>2,383,371</td>
<td>2.53</td>
<td>23</td>
</tr>
<tr>
<td>2000</td>
<td>2,001,516</td>
<td>2.12</td>
<td>25</td>
</tr>
<tr>
<td>2001</td>
<td>1,652,845</td>
<td>1.75</td>
<td>27</td>
</tr>
<tr>
<td>2002</td>
<td>1,334,322</td>
<td>1.41</td>
<td>28</td>
</tr>
<tr>
<td>2003</td>
<td>1,050,567</td>
<td>1.11</td>
<td>29</td>
</tr>
<tr>
<td>2004</td>
<td>801,406</td>
<td>0.85</td>
<td>30</td>
</tr>
<tr>
<td>2005</td>
<td>594,303</td>
<td>0.63</td>
<td>31</td>
</tr>
<tr>
<td>2006</td>
<td>437,034</td>
<td>0.46</td>
<td>31</td>
</tr>
<tr>
<td>2007</td>
<td>330,779</td>
<td>0.35</td>
<td>31</td>
</tr>
<tr>
<td>2008</td>
<td>266,230</td>
<td>0.28</td>
<td>32</td>
</tr>
<tr>
<td>2009</td>
<td>226,333</td>
<td>0.24</td>
<td>32</td>
</tr>
<tr>
<td>2010</td>
<td>198,928</td>
<td>0.21</td>
<td>32</td>
</tr>
<tr>
<td>2011</td>
<td>177,588</td>
<td>0.19</td>
<td>32</td>
</tr>
<tr>
<td>2012</td>
<td>159,319</td>
<td>0.17</td>
<td>32</td>
</tr>
</tbody>
</table>

<sup>1</sup> Actual numerical estimate

<sup>2</sup> Rounded to nearest integer based on cumulative total of actual numerical estimates

The previous analysis compared the side-impact fire performance of the GM and Ford pickups in terms of occupant fatalities. To eliminate the effects of multiple occupancy, so that only vehicle fire performance is measured, the updated Partyka report also includes an analysis based the number of vehicles involved in crashes in which at least one occupant fatality occurred in the vehicle being analyzed. The methodology is identical to that previously discussed. The increase in the number of subject vehicles involved in fatal side MHE=fire crashes compared to the Ford truck is 0.68 vehicles per million registered vehicle-years (Appendix A1, page 8). For vehicles impacting the side of the subject vehicles
compared to the Ford trucks, the increase in the number of vehicles in fatal crashes in which $MHE=\text{fire}$ was 0.02 (Appendix A4, page 20), for a total of 0.70 incremental side-impact fatal crashes where the $MHE=\text{fire}$ per million registered vehicle-years. Thus, given the 4.8 million subject vehicles on the road as of July 1, 1994, ODI estimates that, if past trends continue, the increased risk of fire in those vehicles will result in approximately three to four additional fatal, side-impact $MHE=\text{fire}$ crashes in 1994.

N.2. Validity of FARS Coding

In its July 19 and August 10, 1993, responses to ODI information requests, GM identified a number of examples of FARS cases involving side-impact collisions with fire that GM believes were incorrectly coded or are not relevant to the alleged defect. GM provided this information to support its contention that FARS data do not provide a reliable basis for analyzing the crashworthiness of the fuel system in the subject vehicles. GM provided narrative descriptions of alleged errors in five categories:

1. Not a 1973-1987 C/K pickup truck;
2. No fire in the C/K pickup, or fire originating in other vehicle;
3. Engine compartment fire;
4. Fuel system not as designed; and
5. No side impact.

Of the 168 fatal, side-impact, fire-involved crashes involving 1973-1987 GM subject vehicles from 1975 to 1991, for which matching registration data exist, GM identified 17 FARS cases (10 percent of the total) that it believes fit into at least one of the above five categories. GM provided information based on police reports, photographs, witness statements, rescue squad documents, etc., to support its claim in the five respective categories that:

1. 1 crash involved a GM pickup truck built in the 1964-1966 time frame;
2. 5 crashes either involved no fires (3 crashes) or involved fires that started in another vehicle (2 crashes);
3. 6 crashes involved engine compartment fires in the GM truck;
4. 3 crashes involved fires in vehicles that had aftermarket fuel tanks added; and
5. 2 crashes were not side impacts.

ODI has reviewed the GM analysis and agrees that certain crashes appear to have been miscoded. However, none of the 17 FARS cases identified by GM were coded as $MHE=\text{fire}$. Since the agency's data analysis focused on crashes where the $MHE=\text{fire}$, the FARS errors identified by GM did not have any significant effect on the outcome of that analysis. Additionally, in the absence of any indication that fatal crashes involving the subject vehicles were coded differently from such crashes involving Ford pickups, it is logical to assume that coding errors affected different vehicles similarly, thus reducing any effects on comparisons of relative performance among vehicles. Thus, the fact that there are coding errors in the FARS database does not mean that FARS is an inappropriate database for estimating incremental fatalities associated with or caused by fire in the subject vehicles.
The coding of MHE in FARS is determined by a FARS analyst based on a review of the FARS and available medical reports, but in most instances without the benefit of an autopsy report, since autopsies are not routinely conducted on fatally injured motor vehicle crash victims. GM challenged the accuracy of the FARS MHE coding in its April 30, 1993, response to ODI’s April 9, 1993 recall request letter. In that response, GM detailed the results of its review of the Multiple Cause of Death (MCOD) data collected by the National Center for Health Statistics with respect to side-impact fatal accidents in FARS involving 1973-1987 full-sized GM pickup trucks in which there was a post-crash fire. The MCOD file contains data concerning deaths occurring in the United States since 1973, with the exception of calendar years 1981 and 1982. Information available in the MCOD database includes the underlying cause of death, with a maximum of 19 additional contributory causes. The MCOD coding is based on information available on the Certificate of Death, and the coding is done by the individual states. Unless data are missing or conflicting on the Certificate of Death, no attempt is made during MCOD coding to obtain additional information. The cause and underlying causes of death reported on the Certificate of Death can be entered by a variety of persons, including doctors, coroners, medical technicians, and funeral directors. Some Certificates of Death are prepared after an autopsy is performed and others are not.

GM submitted an analysis of 48 fatal, fire-related crashes involving 1973-1987 full-sized GM pickup trucks in calendar years 1979 through 1988 where the FARS MHE code was fire. GM noted that in 23 of the cases the MCOD coding was "fire injury" (including various additional contributing causes, e.g., shock, fractures and contusions, asphyxia, etc.), in 16 of the cases the MCOD coding was trauma, and in 9 of the cases the MCOD coding was "both fire and trauma injury." Using only the 39 MCOD cases where a single cause of death was listed, GM’s analysis shows that in 23 cases (59 percent), the fatal injuries were attributed to fire.

In response to a request from ODI, on August 10, 1993, GM provided an analysis of 44 MCOD matches with fatal, fire-involved crashes of 1973-1987 full-sized GM pickup trucks where the crashes occurred in calendar years 1979 through 1988, and the FARS MHE code was "other than fire" (i.e., trauma). GM stated that in 12 of these cases, the MCOD coding indicated that the cause of death was fire. In 20 of these cases, the MCOD coding indicated that the cause of death was other than fire. In another 12 cases, GM stated that the cause of death was "both fire and non-fire injuries." Using only the MCOD cases where a single cause of death was listed, GM’s analysis indicates that in 12 of 32 cases (38 percent), the fatal injuries were attributed to fire. Thus, there are differences between MHE coding and MCOD coding for both the "fire" and "trauma" categories that tend to counterbalance each other, suggesting that the MHE coding is a reliable indicator of the cause of death in fire-related crashes.

A comparison of the GM findings using MCOD data with ODI’s analysis of FARS and autopsy data appears in section N.4 of this Report.
N.3. GM/FaAA Analyses of FARS Data

GM contracted with FaAA to assess the risk of post-collision fires in the subject vehicles compared to the risk of similar events in comparable vehicles. Vehicle groups studied were Chrysler, Ford, Nissan and Toyota pickups, as well as the "average" passenger car and the "95th percentile" passenger car.

FaAA examined FARS data and also analyzed several state accident databases. FaAA used data from the six states that utilize the coding variables required to identify vehicle types, collision fires, and area of impact. FaAA analyzed the aggregate data for the 1973-1991 time period, and also disaggregated the data into seven model year groupings, based on what it believed were significant changes in the fuel system of the subject vehicles. FaAA concluded that the side-collision fire rates for the subject vehicles are "generally similar" to the comparison vehicles in collisions of all severity reported in the state data files. FaAA acknowledged that in fatal, fire-involved, side collisions, the fire occurrence rate of the subject vehicles is "generally higher" than other pickups, but asserted that the subject vehicles are not "greatly disparate" from the comparison vehicles.

The initial version of this FaAA analysis, entitled "Analysis of Light Duty Motor Vehicle Collision Fire Rates," was submitted with GM's October 9, 1992 response to ODI's first information request (DP Exhibit 3). This initial FaAA analysis compared GM full-sized pickup trucks with Ford and Dodge pickup trucks of all sizes. GM provided an additional FaAA submission on November 25, 1992, in which only comparably sized pickup trucks were analyzed (DP #33 and #33a).

GM's analysis of FARS data is generally consistent with ODI's. GM's November 25, 1992, analysis indicates that the subject vehicles have a rate of fire occurrence that is 2.7 times greater than that of comparable Ford pickup trucks in fatal side-impact crashes and a rate that is four times greater than that of comparable Ford pickup trucks in fatal side crashes where the MHE=fire.

In response to ODI's recall request letter, GM provided additional analyses of FARS data. Although GM did not dispute the 3.5 to 1 MHE=fire fatality rate ratio as computed from the 1979-1990 FARS data, it claimed that this ratio does not indicate that the subject vehicles present an unreasonable risk of post-crash fires. In support of this claim, GM presented a series of vehicle fire rate comparisons in an effort to show that many other pairs of vehicles experience differences in the rate of fire-related fatalities that are greater than the difference between GM and Ford pickups.

In its analysis, for each make and model considered, GM divided the number of vehicles involved in a fatal crash in which a fire occurred by the number of registered vehicle-years of that make and model. In ODI's view, this approach has several shortcomings. First, the fire rates calculated by GM include all fatal crashes in which fire occurred, even though in many cases the fire was not the cause of death and might not have posed a significant threat to occupant safety. ODI's analysis focused on MHE=fire crashes, which are a subset of fire occurrence crashes and represent crashes in which fire is the most harmful occurrence (as
opposed to mechanical trauma forces). ODI believes that in this investigation, where the pertinent issue is whether there is an unreasonable risk of fire that results in occupant death or injury, fire occurrence crashes are not as relevant as MHE=fire crashes.

Second, in making its vehicle-to-vehicle comparisons, GM used registered vehicle-years as the measure of exposure. In instances in which the vehicles being compared are driven in a similar manner by similar types of drivers, as is the case with the subject vehicles and Ford full-sized pickups (see section N.6, below), this measure of exposure is satisfactory. However, in many, if not most, vehicle-to-vehicle comparisons, this exposure measure allows the effects of driver behavior and demographics on crash involvement to bias the results. For example, if a particular make or model of vehicle is driven by drivers with a high crash involvement frequency compared to another make or model with a similar design, that vehicle would almost certainly have a higher number of crashes with fire, even if there were no vehicle-related differences. Such effects can be very large, particularly when different types of vehicles are compared, making it difficult or impossible to accurately assess the contribution of a vehicle’s design to its post-crash fire performance.

There are two other factors that undercut the force of this GM statistical analysis. Although the data indicate that some vehicle pairs have greater differences in rates of fire-related fatalities than the difference between the GM and Ford full-sized pickups, there are no identifiable engineering or design bases for the differences, as there is here. In addition, in none of the examples identified by GM was there a history of corporate awareness of a safety problem like there is here, as described in section P of this report.

Based on these considerations, the GM approach does not provide an adequate assessment of the contribution of vehicle factors to post-crash fires that result in occupant casualties.

N.4. Autopsy Data

Since the FARS MHE code was an important component in ODI’s statistical analysis of the fire risk associated with the alleged defect, and GM challenged the validity of that code, ODI reviewed autopsy reports to examine whether the FARS MHE code was an accurate representation of the actual cause of death in fatal side-impact crashes involving fire in the subject vehicles.

ODI reviewed all available autopsy reports, 74 in all, involving occupants of the subject vehicles who died in side impact crashes that resulted in a fire. Since such reports are generally maintained in the individual states’ FARS files, and these files are only maintained for several years, there is a limited number of available reports available through FARS. Other such reports were received from GM in response to ODI information requests.

ODI believes that an autopsy is the best means of accurately determining the actual cause of death. Unless based on an autopsy, Certificates of Death, Medical Examiner Reports, Coroner Reports, etc., are a far less reliable indication of the actual cause of death. While autopsies generally give primary and secondary causes of death, only the primary (or first listed) cause was used in this analysis. In some instances where a copy of the autopsy was
not available, but the Certificate of Death noted that an autopsy had been performed, the primary cause of death from the Certificate of Death was used.

Of the 74 cases reviewed, 49 involved crashes where the FARS MHE code was fire, and 25 involved accidents where the FARS MHE code was other than fire; i.e., crash force trauma. The primary cause of death based on the autopsy matched the FARS MHE code in 48 cases (65 percent). Of these 48 cases, 36 were cases where the FARS MHE code was fire and the autopsy indicated that fire was the cause of death. In the other 12 cases, the FARS MHE code was trauma and the autopsy indicated that trauma was the cause of death. Of the remaining 26 cases; i.e., those where the FARS coding did not match the autopsy results, there were 13 instances where the FARS MHE coding indicated other than fire, but the autopsy reported that fire was the actual cause of death, and 13 occurrences where FARS coding indicated fire, but the cause of death was trauma. Table 5 presents the distribution of the 74 cases.

<table>
<thead>
<tr>
<th>Autopsy Cause of Death</th>
<th>FARS Coding</th>
<th>TOTAL</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Fire</td>
<td>Trauma</td>
</tr>
<tr>
<td>Fire</td>
<td>36</td>
<td>13</td>
</tr>
<tr>
<td>Trauma</td>
<td>13</td>
<td>12</td>
</tr>
<tr>
<td>TOTAL</td>
<td>49</td>
<td>25</td>
</tr>
</tbody>
</table>

These data indicate that in crashes in which a fire occurred and the FARS coding is MHE=fire (49 cases), the cause of death was fire according to an autopsy for 73 percent (36/49) of the cases. (The GM analysis using MCOD data yielded a figure of 59 percent). Similarly, for those cases in which the FARS coding was MHE=trauma (25 cases), the autopsy indicated that fire was the cause of death in 52 percent (13/25) of the cases. (The GM analysis using MCOD data yielded a figure of 38 percent.) Although the correspondence of FARS MHE codes to autopsy results is not perfect, the differences go in both directions. On balance, the available information indicates that, for fatal crashes involving fire, the MHE code in FARS provides a reliable measure of the number of such fire-related fatalities in which fire was the cause of death.

The complete analysis of the above data, including an analysis supporting the use of MHE=fire as an accurate measure of fatalities caused by fire and a listing of reviewed autopsy reports, appears in the public file for this investigation.
N.5. The Usefulness of State Accident Data

GM has argued that state data files (databases containing records of a state's police-reported crashes) are superior to FARS as a data source for assessing fire performance. In state data, the measure of exposure is the number of reported collisions. The measure of interest is the number of specific types of events, e.g., crashes with fires, per 1,000 collisions. GM states that by comparing performance on a per collision basis rather than using other exposure measures, such as the number of registered vehicles, differences due to driver exposure effects are eliminated.

NHTSA recognizes that state data files are valuable in assessing numerous safety issues, and the agency will continue to use them where appropriate. However, the usefulness of state files or other crash data sources depends on the safety issue to be addressed. ODI believes that state accident data do not provide sufficient insight into the relationship between the fuel tank design in the subject vehicles and fire occurrence in crashes. Since the vast majority of police-reported crashes occur at the lower end of the crash severity spectrum, fire occurrence differences due to the loss of fuel tank integrity in relatively high crash severity events—which is where differences between GM and Ford fuel tank performance would appear—would not be evident in state accident data. That is, in state data, the relatively low number of higher crash severity events is overwhelmed by the high frequency of lower crash severity events, some of which can result in fires due to factors other than the loss of fuel tank integrity. Thus, any differences in fire occurrence at higher severities due to the loss of fuel tank integrity would be masked when comparing fire occurrence rates over the entire crash severity spectrum covered by the state databases.

Data from the National Accident Sampling System (NASS) demonstrate this phenomenon. NASS is a sampling of police-reported towaway crashes (those crashes in which the damage to the vehicle was severe enough to require towing) of all crash severities involving "light vehicles" (defined as passenger cars, light trucks and vans with a GVWR of 8,500 lbs or less). Table 6 shows, as percentages, for all passenger cars, light trucks, and vans, the portion of side crashes that occur in each crash severity range; the portion of those side crashes in each severity range that involve fire; and the product of those two in each speed range, which is the ratio of the side crashes with fire within each severity range to the total number of side crashes. Crash severity is defined as the estimated speed change in the crash, i.e., delta-V, derived from NASS data. Thus, in a state that reported data on all towaway side impact crashes, an overall fire rate of 0.35 percent would be expected.

If these vehicles had a significantly higher fire occurrence rate due to fuel tank integrity loss in crashes in the high range of delta-V, the overall fire rate would not noticeably change. For example, if the fire occurrence rate in 40-49 mph delta-V side crashes increased by a factor of 2.8, from 3.76 percent to 10.53 percent, the percentage of all side crashes with fire in the 40-49 mph delta-V category would increase from 0.0075 percent to 0.0211 percent, but the overall fire rate in side impacts would only increase from 0.35 percent to 0.36 percent. Thus, a 2.8 times greater fire risk at this higher crash severity would result in only a 0.01 percent increase in the overall fire rate in side impacts.
Table 6. Fire and Crash Severity for Light Vehicle Side Crashes Where the Crash Severity was Known (1979-1986 NASS Towaway Data)

<table>
<thead>
<tr>
<th>Speed Change Delta-V, mph</th>
<th>(1) Side Crashes in Crash Severity Range</th>
<th>(2) Side Crashes with Fire in Severity Range</th>
<th>(1) x (2) Side Crashes with Fire in Severity Range</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Total Side Crashes</td>
<td>Side Crashes in Speed Range</td>
<td>Total Side Crashes</td>
</tr>
<tr>
<td>0-9</td>
<td>40.99%</td>
<td>0.08%</td>
<td>0.0323%</td>
</tr>
<tr>
<td>10-19</td>
<td>50.14%</td>
<td>0.45%</td>
<td>0.2261%</td>
</tr>
<tr>
<td>20-29</td>
<td>7.55%</td>
<td>0.96%</td>
<td>0.0729%</td>
</tr>
<tr>
<td>30-39</td>
<td>1.07%</td>
<td>0.94%</td>
<td>0.0101%</td>
</tr>
<tr>
<td>40-49</td>
<td>0.20%</td>
<td>3.76%</td>
<td>0.0075%</td>
</tr>
<tr>
<td>50+</td>
<td>0.05%</td>
<td>0.00%</td>
<td>0</td>
</tr>
<tr>
<td></td>
<td>100.0%</td>
<td>0.3489%</td>
<td>0.35%</td>
</tr>
</tbody>
</table>

This example demonstrates why state data are not a valid measure for assessing the role of fires due to loss of fuel integrity in this defect investigation. Since fuel tank integrity is generally not compromised until high crash severities are reached, state data are not useful in comparing fuel tank-related fire performance differences among vehicles. If state data could be disaggregated, so that only crashes above the level of crash severity that is associated with the potential for loss of fuel tank integrity were considered, state data could be an appropriate database. However, such a crash severity disaggregation is not possible with state data.

It is also appropriate to consider whether the state accident data submitted by GM provide a representative data sample, given that the alleged defect is a national safety concern. That is, when using accident data from a limited number of states, it is necessary to determine whether those data represent national accident conditions.

GM’s most comprehensive analysis of state data appears as Appendix O to GM’s August 10, 1993, submission. This document presents accident statistics from nine states: Alabama, Arkansas, Florida, Idaho, Illinois, Maryland, Michigan, North Carolina, and New York. Included in this database was information on the number of side-impact and total crashes in the following categories: all reported crashes, incapacitating injury crashes, fatal crashes, post-collision fire-involved crashes, and post-collision fire-involved fatal crashes. GM reported a total of 13 side fire-involved fatal crashes out of a total of 241 side-impact fatal crashes in six of those states. (GM did not provide information regarding location of impact for three of the nine states.) This yields a fire occurrence rate of 5.4 percent (13/241) in fatal side-impact crashes. The updated Partyka analysis of national data from FARS.
indicates that 8.6 percent of the side-impact fatal crashes involving the subject vehicles had a post-crash fire (Appendix A1, page 7). Thus, the national fire rate in side-impact fatal crashes is 59 percent greater than that rate in the six states analyzed by GM.\textsuperscript{10} The fact that GM's state data yield fatal fire occurrence rates for the subject vehicles that are substantially lower that the national rates indicates that these limited state data do not provide a valid representation of the nationwide experience with respect to side-impact, fire-related fatal crashes involving the subject vehicles. Therefore, even apart from their doubtful utility in addressing issues related to post-crash fuel system integrity, they do not provide a valid basis for assessing the overall fire occurrence experience of the subject vehicles.

N.6. The Effect of Driver Demographics and Behavior

In its August 10, 1993 submittal, GM stated that "non-vehicular factors must account for all or most of the differential" in post-crash fire rates between GM and Ford full-sized pickups. Relying primarily upon state data, GM claims that this difference is "... chiefly a reflection of driver or exposure difference and not a vehicle design or performance difference."

To assess the validity of GM's assertion, ODI conducted several analyses. First, if the demographics and behavior of drivers of the subject vehicles were responsible for the increased number of fatalities due to fire in side-impact crashes in the subject vehicles compared to the Ford pickups, this increase would be expected in both the 1973-1987 and the 1988-1992 model year groups.\textsuperscript{11} The number of side-impact MHE=fire occupant fatalities for calendar years 1979-1993 are presented in Table 7, along with the rates of side-impact MHE=fire occupant fatalities per million registered vehicle-years for various model year groupings.

\textsuperscript{10} In all crash modes, GM's nine-state data show that there were 52 fires in 1,384 fatal crashes involving the subject vehicles, yielding a fire occurrence rate of 3.8 percent in all fatal crashes. National data from FARS yield a fire occurrence rate in all fatal crashes involving the subject vehicles of 6.5 percent (Appendix A1, page 6), which is 70 percent greater than the nine-state rate.

\textsuperscript{11} ODI focussed its statistical analyses on a comparison of the post-crash fire performance of the subject vehicles to that of MY 1973-1987 Ford full-sized pickups, primarily on the basis that those Ford pickups were a product of the construction, design, and materials technologies in use during the period in which the subject vehicles were produced. However, in considering the possible effect of driver demographics and driver behavior on fatal fire rates, it is clearly appropriate to compare the fire performance of the subject vehicles to that of the post-1987 C/K pickups, as well as to the fire performance of pre- and post-1987 Ford pickups. It is also noteworthy that although GM incorporated numerous design changes into its MY 1988 pickups, the primary difference for fuel system integrity purposes was the shift of the fuel tanks inside the frame rails.
Table 7. Comparison of Side-Impact MHE=Fire Occupant Fatality Rates for Various Model Years of Ford and GM Full-Sized Pickups (FARS Data 1979-1993)

<table>
<thead>
<tr>
<th>Make</th>
<th>Model Years</th>
<th>MHE=Fire Occupant Fatalities</th>
<th>MHE=Fire Occupant Fatalities per Million Registered Vehicle Years</th>
</tr>
</thead>
<tbody>
<tr>
<td>GM</td>
<td>1973-1987</td>
<td>120</td>
<td>1.40</td>
</tr>
<tr>
<td>Ford</td>
<td>1973-1987</td>
<td>31</td>
<td>0.41</td>
</tr>
<tr>
<td>GM</td>
<td>1988-1992</td>
<td>3</td>
<td>0.36</td>
</tr>
<tr>
<td>Ford</td>
<td>1988-1992</td>
<td>3</td>
<td>0.41</td>
</tr>
</tbody>
</table>

For the 1988-1992 model year group in comparison to 1973-1987, the location of the Ford fuel tank remained the same -- inside the frame rails -- while the GM fuel tank was moved inside the frame rails. For Ford, the occupant fatality rates for the two model year groupings are identical (0.41 for both the 1973-1987 group and the 1988-1992 group). However, the rate for the 1988-1992 GM pickups is significantly lower than that of the subject vehicles, declining from 1.41 to 0.36 occupant fatalities per million registered vehicle-years.

These data provide the most compelling evidence that the substantial difference in the rate of MHE=fire fatalities in side-impact crashes involving 1973-1987 GM and Ford full-sized pickups is due to fuel tank location and design rather than demographic and behavioral differences between drivers of these pickups or other exposure differences. If such factors were significant, the rate of occupant fatalities for the 1988-1993 GM pickups should be similar to that of the 1973-1987 GM pickups, and be far in excess of the rate for the 1988-1993 Ford pickups. Neither of these relationships is reflected in the data. Rather, these data show that there was a substantial decrease in the side-impact MHE=fire occupant fatality rate for the GM pickups when the fuel tanks were moved inside the frame rails. Thus, they provide further support for a determination that the increased fatalities due to burns from side-impact crashes involving the subject vehicles are due to the design and location of their fuel tanks.

In a further effort to assess GM’s claims regarding alleged demographic differences, ODI also reviewed available state data to assess whether the subject vehicles were involved in a disproportionate number of crashes per registered vehicle compared to full-sized Ford pickups across the entire crash spectrum. As noted above, because fire-related fatal crashes are very rare and represent a small portion of total crashes, care must be taken in using state accident data to analyze fire-related fatal crashes. Because they cover the entire crash severity spectrum, however, state data may be used in assessing whether there are differences in the number of collisions per registration between the subject vehicles and Ford pickups.
<table>
<thead>
<tr>
<th>State</th>
<th>Year</th>
<th>Total RVY (Registered Vehicle-years)</th>
<th>All Crash Involved Vehicles</th>
<th>Crash Involved Vehicles per 10,000 RVY</th>
<th>Ratio of GM-to-Ford</th>
<th>Side Crash Involved Vehicles</th>
<th>Side Crash Involved Vehicles per 10,000 RVY</th>
<th>Ratio of GM-to-Ford</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>GM 1973-1987</td>
<td>708,183</td>
<td>27,440</td>
<td>387</td>
<td>1.02</td>
<td>12,650</td>
<td>178</td>
<td>1.02</td>
</tr>
<tr>
<td></td>
<td>GM 1973-1987</td>
<td>2,374,567</td>
<td>140,797</td>
<td>593</td>
<td>1.01</td>
<td>69,568</td>
<td>293</td>
<td>0.99</td>
</tr>
<tr>
<td></td>
<td>GM 1973-1987</td>
<td>829,229</td>
<td>18,827</td>
<td>227</td>
<td>1.06</td>
<td>8,747</td>
<td>105</td>
<td>1.01</td>
</tr>
</tbody>
</table>
Although the data on collisions per registration are not extensive, some states have sufficient data for the relevant years to shed light on this issue. By obtaining the number of vehicles in crashes and the number of vehicle registrations over a period for both GM and Ford trucks, the rate of collisions per 10,000 registered vehicle-years can be calculated. Table 7 presents the number of crash-involved vehicles and registered vehicles for both "all" and "side" crashes in the three states for which adequate data are available in the calendar years noted.

The fourth column presents the ratio of all crashes per 10,000 registered vehicle-years for GM compared to Ford for the three states. As shown, the ratio ranges from 1 to 6 percent higher for GM compared to Ford. The seventh column presents the ratios of crashes per 10,000 registered vehicle-years for GM compared to Ford in side crashes. This ratio ranges from 1 percent lower to 2 percent higher for GM.

If there were significant differences in the behavior of drivers between these two vehicles, such that the GM drivers were more susceptible to crash involvement, these ratios would reflect such a difference. The consistency of the ratio among the states leads to the finding that driver characteristics do not produce a substantially different degree of crash involvement for the GM and Ford trucks.

ODI also examined insurance data to assess possible driver effects on crash involvement. The Highway Loss Data Institute (HLDI) retains information on the collision claims filed by drivers of various make/model vehicles. The parameters available include the number of collision insurance claims filed per insured-vehicle-year (a measure of exposure), as well as the average loss payment per claim. These data are helpful in assessing any effects of driver demographics and behavior on overall crash involvement. First, it is logical that if drivers of GM pickups exhibited behavior which increased their risk of crash involvement, the number of collision claims per insured-vehicle-year for the subject vehicles would be elevated compared to that of Ford pickups. Second, if the drivers of GM pickups were involved in, on average, more severe crashes than drivers of Ford pickups, the average cost per claim for the GM trucks would be higher. These HLDI data for model year 1979-1987 full-sized GM and Ford pickups are presented in the public file. The values for the data are normalized to passenger cars, with 100 representing the average passenger car value. The data do not indicate that drivers of GM pickup trucks are involved in more crashes, or more severe crashes, compared to drivers of Ford pickups.

Because of the deficiencies and limitations of the state databases relied upon by GM, ODI analyzed FARS data to assess whether demographic and behavioral characteristics, which GM claimed were the cause of the difference in side-impact fire fatality rate between GM and Ford trucks, were reflected in that data.12 For example, Table 9 presents the number and percentage of fire-involved side-impact driver fatalities, by age of driver, in the GM and Ford pickup trucks.

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12 Susan Partyka. Fire and other Factors in Crashes with Driver Fatality in Certain Full-Sized American Pickup Trucks, NHTSA, November 17, 1993. This report appears in the public file for this investigation and excerpts appear in Appendix F of this Report.
Table 9. Distribution of Driver Fatalities in Side-Impact Crashes by Driver Age

<table>
<thead>
<tr>
<th>Driver Age</th>
<th>GM</th>
<th>Ford</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Total Driver Fatalities</td>
<td>Fire-Involved Driver Fatalities</td>
</tr>
<tr>
<td>0-14</td>
<td>6</td>
<td>0</td>
</tr>
<tr>
<td>15-19</td>
<td>277</td>
<td>36</td>
</tr>
<tr>
<td>20-24</td>
<td>366</td>
<td>43</td>
</tr>
<tr>
<td>25-44</td>
<td>888</td>
<td>89</td>
</tr>
<tr>
<td>45+</td>
<td>794</td>
<td>56</td>
</tr>
<tr>
<td>All</td>
<td>2,331</td>
<td>224</td>
</tr>
<tr>
<td></td>
<td>1,838</td>
<td>77</td>
</tr>
</tbody>
</table>

These data indicate that, for both GM and Ford trucks, the percentage of drivers killed in side-impact crashes in which fire occurred generally decreases as the age of the driver increases. However, the ratio of GM-to-Ford driver fire-involved fatality rates in the different age groups is consistently between 2.2 and 2.5, with an average value of 2.3. The only way this consistent relationship could be related to non-vehicle factors is if, within each age group, drivers of the GM trucks drove their vehicles differently than drivers of the Ford trucks drove their vehicles. Thus, differences in age among drivers of GM and Ford trucks in fatal crashes cannot explain the differences between the GM and Ford fatal side-impact fire rates.

Additional analyses are included in the November 17, 1993, Partyka report for other factors that GM asserted were relevant, including alcohol use and posted speed limit. As with the driver age analysis, the data indicate that the percentage of fire-involved crashes in GM trucks was higher compared to Ford trucks in both alcohol-involved and non-alcohol-involved crashes, as well as at all speed limits.

These analyses indicate that the GM driver fatalities tended to be slightly younger than the Ford driver fatalities and more of them were reported to have been drinking, based on cases for which alcohol involvement was reported. This difference suggests that the GM pickup trucks might be driven less cautiously, but it is not possible to describe general vehicle use from fatal crash data alone. There was little difference in the types of roads on which these vehicles were used, 66 percent of both Ford and GM pickup truck driver fatalities occurred with a speed limit of at least 55 mph, and 78-79 percent of these crashes occurred in rural areas. Most important, the analyses demonstrate that the percentage of driver fatalities that involved fire is greater for GM pickup trucks (compared to Ford pickup trucks) in every
category of driver age, alcohol use, speed limit, and urbanization. Thus, while driver risk-taking might contribute to some degree to the higher rate of fire involvement in fatal crashes for GM pickup trucks, the data do not support GM’s contention that driver demographics and behavioral differences account for the differences between GM and Ford full-sized pickup trucks in fatal crashes involving fire.

In a further effort to support its assertions about the effect of demographic differences, GM submitted a paper entitled "Exposure Severity, Crash Severity, and Crash Outcomes," dated March 1994 (EA 54827). The paper asserts that 1973-1987 GM full-sized pickup trucks have a larger portion of crashes in the crash severity range of 15 mph delta-V and higher compared to 1973-1987 Ford pickup trucks. The paper suggests that this apparent crash severity exposure difference could explain the difference in the fire-related fatality rates between GM and Ford trucks, rather than differences in fuel tank location in the two pickup trucks.

To begin with, the NASS data sample on which this paper was based was not designed to be utilized in comparisons of particular vehicles, in part because of its relatively small size. In any event, the ODI analysis of non-vehicle factors described above demonstrates that the differences in post-crash side-impact fire rates cannot be explained by such non-vehicle factors. Thus, even if it were true that the subject vehicles were somewhat more likely than the Ford pickups to be involved in high severity crashes, such a difference could not explain the extent of the differences in the vehicles' fire-related fatality rates or MHE=fire fatality rates in side-impact crashes or in all crashes.

N.7. Burn Injury Data

In addition to its analysis of fatal accidents, ODI also examined the issue of burn injuries arising from post-crash side impact fires involving the subject vehicles.

As of December 31, 1993, ODI had reports reflecting a total of 158 non-fatal burn injuries (in crashes occurring from 1973-1993) to occupants in side-impact post-crash fires involving the subject vehicles. Of the 158 persons injured, 129 were occupants of the GM truck, and 29 were occupants of other vehicle(s) involved in the accident. Of the 129 occupant injuries, 104 occurred during the period 1979-1993.

To ascertain the relationship between burn injuries and burn fatalities in the subject vehicles, ODI divided the number of occupant burn injuries from side-impacts during 1979-1993 (104) by the number of MHE=fire side-impact occupant fatalities during the same time period (139), resulting in a ratio of 0.75. That is, the data indicates that there have been three burn injuries to occupants of the subject vehicles from side-impact crashes for every four MHE=fire side-impact occupant fatalities. Applying this ratio to the estimated five additional occupant fatalities in the subject vehicles expected in 1994 results in an estimated 3.4 additional burn injuries in the subject vehicles compared to the Ford pickups in 1994.
ODI also reviewed a recent analysis of eleven years of NASS data involving the light motor vehicle fleet to see if it confirmed this relationship. Extrapolations from the NASS data indicate that there were an estimated 3,083 survivors of crashes with AIS\(^4\) 2-5 burns and 7,972 fatalities with burns. For those fatalities where a medically-determined cause of death was reported, over half (57 percent) of the fatalities with burns died from their burns. If this proportion were consistent throughout the NASS sample, 4,544 of the fatalities with burns would have died due to fire (0.57 x 7,972 = 4,544). Dividing this number into the number of burn injuries in all crashes results in a burn injury-to-burn fatality ratio of 0.68 for the entire light vehicle fleet, which is close to the 0.75 ratio computed in the preceding paragraph.


\(^{14}\) AIS (Abbreviated Injury Scale) is a graduated scale system for assigning a numeric value to indicate the severity of an injury. The scale range is from one (minor) to six (fatal).
O. CRASH SEVERITY

The laboratory tests performed for ODI indicated that in a side crash in which a full-sized 1991 Chevrolet Caprice struck a subject vehicle at 50 mph, there was fuel tank leakage from the subject vehicle. An identical test with a Ford truck did not result in tank leakage. The ODI crash testing also demonstrated that a variety of crash parameters affect the likelihood of fuel tank leakage, including crash speed, mass of the impacting object, geometrical shape of the impacting object at the collision interface, and stiffness of the impacting object.

The 50-mpg impact by the Caprice resulted in a speed change during the crash, known as delta-V, of approximately 24 mph for the GM truck. This is considerably higher than the 9-mpg delta-V that results from an FMVSS No. 301 side-impact barrier test of a GM pickup. Additionally, the energy absorbed by the GM truck in the 50-mpg test, which is also a measure of the severity of a crash, was considerably higher than in an FMVSS No. 301 side-impact test. In the 50-mpg Caprice crash tests, the GM truck absorbed approximately 114,000 ft-lbs of energy, compared to approximately 27,000 ft-lbs in an FMVSS No. 301 side-impact test.

Although the ODI crash tests indicated that tank leakage in the subject vehicles occurred at high levels of delta-V and absorbed energy, this did not preclude the possibility that leaks could occur at lower levels. Because laboratory testing to assess the likelihood of fuel tank leakage under all crash conditions would be prohibitively expensive, time consuming, and subject to the variations associated with crash testing, ODI concluded that the best approach to further assess the relationship between crash severity and tank leakage was to review available information about real-world crashes of GM and Ford pickup trucks that had been in side collisions involving fire in which an occupant was fatally injured.

ODI analyzed 135 PARs from fatal, side-impact, fire-involved crashes involving the subject vehicles and 17 such crashes involving comparable Ford pickups. The crashes represent a wide variety of crash conditions, including both vehicle-to-fixed object and vehicle-to-vehicle crashes. The impacting vehicles include various sizes of passenger cars, light trucks, medium trucks, heavy trucks including tractor-trailers, and trains.

The diagrams of the crash scene and the crash description in each PAR were used to estimate pre-impact travel speeds and relative velocity vectors for the vehicles involved. For vehicle-to-fixed object crashes, it was necessary to estimate the speed of the pickup truck at impact in order to calculate the change in velocity (delta-V); i.e., the change in velocity equalled the travel speed. For vehicle-to-vehicle crashes, it was necessary to ascertain the impact speeds

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15 This disparity in the number of crashes analyzed is due to two factors. First, there have been far more side-impact, fire-related fatal crashes involving the subject vehicles. Second, the PARS for crashes involving the subject vehicles were obtained from a variety of sources including FARS, GM, the Association of Trial Lawyers of America, the CAS, and various private attorneys, while those for the crashes involving the Ford pickups came only from FARS.
and weights for both vehicles. These speeds were then used with the weights of the vehicles involved to estimate the delta-V of the pickup truck in each crash.

Figures 4 and 5 present the results of this analysis for GM and Ford pickups, respectively. The figures depict the percentage of fire-related, fatal side-impact crashes within five mph delta-V increments for each of these vehicles. Also shown is the 24 mph delta-V obtained in the ODI 50-mph crash test of a subject vehicle that resulted in a fuel tank leak. This indicates that a 50-mph crash is at the lower end of the range of crash severity necessary to cause a fire due to a fuel tank leak in both the subject vehicles and the Ford pickups; i.e., approximately 65 percent of the GM crashes and 94 percent of the Ford crashes analyzed by ODI had delta-V values above 24 mph.

![Figure 4. Percent of GM Pickup Truck Fatal Side Crashes with Fire, by Crash Severity (Delta-V in mph).](image-url)
Figure 5. Percent of Ford Pickup Truck Fatal Side Crashes with Fire, by Crash Severity (Delta-V in mph).

Figure 6 presents the GM and Ford data together. Because of the limited number of Ford crashes available for analysis, ODI recognizes that the graph of the Ford data may not be a precise reflection of the delta-V experienced by Ford pickups in fire-related fatal crashes. Nevertheless, ODI believes that these graphs provide a valid indication that, in general, the crash severity needed to cause a fire in a fatal side-impact crash involving a Ford pickup is greater than that needed to cause a fire in such a crash involving the subject vehicles.
These data indicate that the average crash severity for the GM truck in fatal side-impact crashes with fire is at a delta-V of 36 mph, while the Ford delta-V average is 55 mph. Thus, while fatal side-impact crashes with fire involving the subject vehicles occur at extremely high levels of crash severity, and at severity levels far in excess of that associated with a FMVSS No. 301 side-impact test, those severity levels are often below those required to create a post-crash fire in the Ford pickups.
P. THE REASONABLENESS OF THE FUEL SYSTEM DESIGN IN THE SUBJECT VEHICLES

The preceding sections of this report demonstrate that there is an increased risk of death and injury due to fire in side-impact crashes involving the subject vehicles compared to the risk of such deaths and injuries in side-impact crashes involving similar pickup trucks with fuel tanks located between the frame rails. Moreover, since that increased risk cannot be attributed to demographic or behavioral factors, it appears to be associated with the side-mounted fuel tank design in the subject vehicles. However, in considering whether that design constitutes a defect that relates to motor vehicle safety within the meaning of the Safety Act, it is necessary to consider whether that design creates an unreasonable risk of deaths and injuries; in other words, whether the increased risk associated with that design is unreasonable under the circumstances.

In addition to the existence and the absolute magnitude of the increased risk, other factors that are relevant to such a reasonableness inquiry are: (1) what GM knew about the safety risk associated with side-mounted fuel tanks at the time it was designing the subject vehicles in the early 1970s, (2) the information regarding the increased risk of the side-mounted tanks that became available to GM during the fifteen years that the subject vehicles were produced, and (3) the availability of alternative feasible fuel system designs that presented a lesser safety risk.

This reasonableness inquiry has elements that are similar to the criteria that are applied by courts in product liability actions; i.e., courts find that a product is "unreasonably dangerous" if a reasonable person would conclude that the danger that could have been avoided, given the information available to the manufacturer and the state of the art at the time, outweighs the financial cost of preventing the danger, the loss of benefits associated with the alternative design, and any new or additional danger created by the alternative design. See generally, Prosser and Keeton on Torts, 5th ed. (1987) at 699; Restatement 2d of Torts, §402A.

P.1 GM'S AWARENESS OF THE POTENTIAL SAFETY CONSEQUENCES OF SIDE-MOUNTED FUEL TANKS

a. Information Available to GM During the Design of the Subject Vehicles

There are a number of internal GM documents dating from the 1960s that reflect GM's awareness that a side-mounted location for the fuel tanks on the subject vehicles had the potential to create a greater risk of post-crash fires than a between-the-frame-rails design. For example, in a 1964 memorandum addressing a variety of safety improvements to be incorporated into the design of the next generation of C/K pickups (at that time scheduled for MY 1967), Alexander Mair, the Executive Engineer for the Chevrolet Truck Department stated, "The fuel tank must be mounted outside the cab and as near the center of the vehicle as practical." EA 053520.
GM's internal design criteria that were in effect when the subject vehicles were being
designed described design features for fuel tank location that called for "sufficient crush
space between the rear bumper and the tank" to avoid a tank rupture in a rear crash and the
avoidance of "puncture-producing surroundings." "Design Direction No. 8-A" (page 00156),
which was applicable to all GM vehicles (including pickup trucks) introduced during or after
MY 1971. While these "design directions" are "objectives" rather than binding
requirements, they demonstrate that GM recognized that vehicles that did not satisfy these
criteria were more vulnerable to post-crash fuel leaks.

The side-mounted location of the fuel tanks in the subject vehicles does not satisfy the spirit
of the first of these criteria, since there is no crush space between the side sheet metal and
the tank.\textsuperscript{16} The design is also inconsistent with the second criterion, since the tanks are
clearly vulnerable to punctures in side crashes, both from objects on a striking object and
from sharp objects surrounding the tank on the trucks themselves. See section M.4 of this
Report.

DD-8-A also provided that maximum fuel leakage amounts for frontal, rear, and side impacts
at 30 mph. GM has consistently claimed that the C/K trucks satisfied this "30-30-30" mph
criterion (see, e.g., GM's October 9, 1992 response, DP #12, at 41, 45, and 46; testimony
of James McDonald in\textit{Moseley v. General Motors}, DP Exhibit 5.5, at 14137-14138).
However, GM did not conduct 30-mph crash tests on production models of the subject
vehicles prior to releasing them for sale, and several of the tests of prototype models with
tanks mounted outside of the frame rails resulted in leaks.\textsuperscript{17} In addition, leaks occurred in at
least two 30-mph side-impact tests that GM performed on these trucks in late 1972 and early
1973, soon after it started selling the subject vehicles to the public.\textsuperscript{18}

The development of the 30-30-30 criterion is discussed in a February 15, 1972 memorandum
prepared by James Steger, a GM engineer (EA 057582). It is also discussed in a 1972 report
by Ronald Elwell, Mr. Steger, and Paul Judson, three GM engineers, which states that fuel
leaks "should not occur" in collisions which produce occupant impact forces below the level
that would cause a fatality in the absence of fire (EA 057590).

\textsuperscript{16} Since the vast majority of vehicles covered by DD-8-A had fuel tanks in the rear, it
refers to the space between the tank and the rear bumper. However, the same safety
considerations would appear to apply to the side-mounted fuel tanks.

\textsuperscript{17} For example, Test C-2509, 9/22/71 (30 mph frontal); Test C-2582, 12/7/71 (15.6
mph side barrier); Test C-2587, 1/4/72 (35 mph car-to-truck impact at 45 degrees).

\textsuperscript{18} Test C-2806, 9/9/72; and Test C-3045, 5/13/73. In addition, in Test C-2807, 9/9/72,
although there was no tank leak, there was a slight leak at the fuel filler cap from a pickup
equipped with a metal shield that appears to cover the bottom and a portion of the sides of
the tank.
b. Information that Became Available to GM During the Time the Subject Vehicles Were Being Produced

The extent of GM's knowledge of the safety risk associated with this design in later years is relevant to this investigation for two distinct reasons. First, GM had the opportunity to revise the fuel system design of the subject vehicles long before it did so in MY 1988, and the reasonableness of its decision not to make such a change is dependent to some degree upon the information available to the company. Second, the extent of GM's ongoing knowledge about the performance of these trucks in side-impact crashes is relevant to the issue of whether GM violated 49 U.S.C. § 30118(c) (formerly section 151 of the Safety Act), which provides that a manufacturer that determines, or in good faith should determine, that its vehicles contain a safety-related defect must promptly notify NHTSA of the defect and provide an appropriate remedy to owners.

The initial indication that the fuel system integrity performance of the subject vehicles was unsatisfactory came soon after the vehicles were initially sold to the public. As noted above, Test C-2806, a 30-mpg side-impact test conducted in early September 1972, resulted in a tank leak. This test, among other things, apparently led GM to consider placing a metal shield around the fuel tank to "provide additional side protection to the fuel tank" of the subject vehicles. See Design Work Order (DWO) 36109-4 (DP Exhibit 6.2, at page 736).

DWO 36109-4 was issued on August 3, 1972, prior to the two September 1972 tests that resulted in leaks. Its original "subject" was "Reinforce Fuel Tank Straps," and the "work to be accomplished" was described as "Redesign fuel tank straps so that a high rate system is provided around the fuel tank side area." Although DWO 36109-4 does not identify the factors that led to its issuance, it may have resulted from two 30-mpg frontal tests of prototype vehicles: C-2369 (no tank leak) and C-2509 (tank leak from sending unit) in which there was tank movement and strap slippage. As demonstrated by the "Design Log" that accompanied the DWO (at page 737), work was not started on the project until September 13, 1972, and before much work had been done, its objective was changed, as indicated in the designer's October 16, 1972 notes (at page 738): "[B.F.] Boehm [who at the time was Assistant Staff Engineer - Chassis within Chevrolet's Truck Division] wants some proposals made for a shield to cover top and side of entire tank. He wants something that will relay impact force to frame if struck on the side." It seems likely that this change in direction was motivated, at least in part, by the tank leak in the September side-impact test.

Following completion of the design work on this DWO, on January 31, 1973, GM tested a MY 1973 Chevrolet C20 pickup truck equipped with the steel shield in a 30 mph side-impact, with no leak (Test C-2949). Notwithstanding the previous test failures, GM did not modify the design of the subject vehicles to equip them with a steel shield, or make any other
product improvement at that time. Mr. Elwell testified in *Moseley v. General Motors* that he was told by George Kendro, the GM engineer in charge of the fuel storage system for the subject vehicles, that James McDonald, who was General Manager of the Chevrolet Division at the time and later President of GM, had "ordered him to stop any further work on those steel shields because it would produce the wrong image to the public...."

GM also performed at least two internal analyses of the post-crash performance of the subject vehicles. The first of these was prepared by F.K. Miller in June 1974, less than two years after they were first sold (EA 053609). Using the limited data available at that time, the analysis compared pre-1973 pickups to the subject vehicles (with respect to fuel leakage as well as other crash aspects). The key finding with respect to the pending investigation is that in accidents where at least one occupant was injured, "The frequency of fuel leaks has not changed. However, given a fuel leak has occurred, the 1973 trucks had more fuel leaks from the fuel tanks than did the pre-1973 pickups."

The second such GM analysis was a study of the post-crash fuel fire performance of 1973-1976 C/K pickups in real-world accidents that was prepared in September 1978 by George Garvil, a member of the Field Accident Research Group within GM's Automotive Safety Engineering Division (EA 053623). The purpose of the study was to assess the relative merits of possible fuel tank locations under consideration for the next generation of C/Ks (which at that time was planned for MY 1981 or MY 1982) based upon a review of accident data. Mr. Garvil concluded that "while the data appear to favor a rear-located tank, it should be considered that a side-located tank...inboard of the frame...might become as effective as a rear-located tank." The report also noted that 19 percent of the side impacts reviewed were judged to have a "high fuel tank leakage potential for outboard side-located tanks. Moving these side tanks inboard might eliminate most of these potential leakers."

Although the report was presented to the GM Design Staff, no action was taken, and no changes were made to the overall design of the trucks until MY 1988.  

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19 As discussed in section G and Appendix A of this Report, GM made several modifications to the design of the subject vehicles during the years they were in production in order to improve their fuel system integrity performance in side impacts. On none of those occasions did GM conduct a recall to improve the performance of the vehicles that had previously been sold to the public. GM asserts that such recalls were not required because the vehicles did not contain a safety defect.

20 Several years later, in January 1983, Mr. Garvil prepared a memo "to correct some misimpressions" created by his 1978 study (DP #14, Attachment 3i, Exhibit 6.8, page 92). In that memo he stated that "it is much less important where the tank is placed than how it is placed. In conclusion, a rear tank location does have the advantage of fewer heavy impacts, but this advantage is not a major one." *Id.* at 93.
In 1981, GM embarked upon a series of 50-mph vehicle-to-vehicle side-impact tests of the subject vehicles under its "Corporate Product Performance Objective" (CPPO) program in an effort to "enhance the ability of the fuel storage system to manage significantly greater levels of energy." See section L.1. These tests clearly demonstrated the vulnerability of the subject vehicles to significant fuel leakage in 50-mph side impacts, even when a variety of "enhancements" were added in an effort to improve post-crash fuel system performance. GM ultimately incorporated three of these enhancements into the trucks beginning in MY 1984, but did not conduct a recall to add them to the earlier models.

Beginning in 1983, there are a number of documents indicating that GM decided to move the fuel tanks inside the frame rails in the next generation of C/K pickups (which did not appear until MY 1988) in order to reduce the likelihood of post-crash fires. For example, at an October 1983 meeting of GM’s Safety Review Board, it was noted that the fuel tank(s) of the new vehicle would be inside the frame rails and that "protection of the fuel system will be the major objective" (EA 063641). Similarly, a December 1983 meeting of GM’s Product Policy Group noted that "the fuel tank will be relocated inside the frame rails, ahead of the rear axle - a much less vulnerable location than today’s tanks" (EA 053655).

Later, in May 1985, after the design of the new C/Ks was well underway, Mike Juris, the chief engineer for that project, advised GM’s President, James McDonald, that the existing design "is subject to intense pressure as a result of litigation due to post crash fuel fed fires. With the tank [of the new truck] located inside the frame rail . . . we are reducing this concern" (EA 053679). Also, a 1988 GM sales brochure for the new C/K pickups stated, "The fuel tanks are mounted inside the frame to reduce the chance of fuel spillage upon side impact" (EA 053703).

It is also noteworthy that, beginning in the mid-1970s, GM had to defend a growing number of lawsuits arising out of post-crash fires in which the side-mounted tank design was claimed to be defective. Although GM consistently opposed such allegations, these lawsuits certainly provided additional notice to GM of a possible problem associated with this fuel system design.

**P.2 The Feasibility of Alternative Designs**

An alternative is considered feasible in the products liability context if a reasonable person would conclude that the danger that could have been avoided, given the technical knowledge available to the manufacturer and the state of the art at the time, outweighs the financial cost of preventing the danger, the loss of benefits associated with the alternative design, and any new or additional danger created by the alternative design.

In applying these factors, there is, first, no doubt that a between-the-frame-rails design for fuel tanks in full-sized pickups was within the state of the art in the early 1970s, as evidenced by the fact that Ford utilized that design in most of its new MY 1973 pickups. (Dodge began to incorporate this design in its pickups as a standard feature two years later.) Moreover, GM considered such designs at the time, but rejected them for marketing reasons.
rather than safety or engineering reasons.\textsuperscript{21} Second, it appears, and GM has not suggested otherwise, that there would have been little or no additional cost associated with a between-the-rails design.

GM has asserted that equipping the subject vehicles with side-mounted tanks led to benefits to its customers that would not have been available with a between-the-rails design (October 9, 1992 response, DP #12, at 41, 44-48). It notes that by retaining a 34-inch frame rail separation, "body builders" could continue to install the same components on new C/K chassis that they had on the previous, pre-1973 version. The company also asserts that, given the limited space between the frame rails resulting from the decision to retain the 34-inch separation, it was necessary to place the tanks outside the frame rails to achieve the fuel capacity (40 gallons) needed to provide the driving range desired by some of its customers. However, beginning in MY 1974, GM offered a between-the-frame-rails 40-gallon fuel tank as optional equipment on its Suburban vehicles, which also had a 34-inch frame rail separation, and considered such a design for the subject vehicles as early as 1971 (see DP Exhibit 6.2, at page 608).\textsuperscript{22}

Finally, there is no evidence that placing fuel tanks inside the frame rails would have created any additional danger. GM has stated that one reason it did not place the fuel tanks between the frame rails and forward of the rear axle was "concerns about placing a fuel tank in close proximity to a spinning drive shaft" (October 9, 1992 response, DP #12, at 47). However, there have been extremely few, if any, fires resulting from such a scenario since the tanks were moved inside the frame rails in MY 1988, and no indication that GM was aware of any such incidents at the time it was designing the subject vehicles.

Q. FINDINGS

1. There are no data on which to conclude that the GM trucks to which FMVSS No. 301 applied, when new, did not comply with the standard.

2. There are no data to indicate a relationship between fuel tank corrosion and increased fire risk in the subject vehicles, either in side impacts or in non-crash incidents.

3. Based on a review of 1979-1993 accident data reflecting the performance of full-sized pickups in side-impact fatal crashes involving fire, occupants of the subject vehicles experienced 2.8 times as many fire-related fatalities (i.e., fatalities in crashes in which a fire occurred) per million registered vehicle-years as occupants of Ford pickups and

\textsuperscript{21} See, in general, GM's October 9, 1992 response, at 44, 46; see also, for example, the testimony of Earl Stepp, chief engineer of trucks for Chevrolet, in Romine v. General Motors (DP #14, Attachment 2, Part F, Exhibit 5.5, at page 18702).

\textsuperscript{22} The fuel tank on the Suburban was behind the rear axle, which is where GM placed the spare tire for the subject vehicles.
2.5 times as many as occupants of Dodge pickups. Where the FARS code indicated that the most harmful event (MHE) of the crash was fire, the GM-to-Ford occupant fatality per million registered vehicle-years ratio is 3.4 to 1, and the GM-to-Dodge ratio is 6.1 to 1.

4. Apart from the basic decision to locate the fuel tanks of the subject vehicles outside of the frame rails, many of the specific features of the design of the fuel storage system and the surrounding area have increased the likelihood of post-crash fuel fires in the subject vehicles.

5. Real-world accident data do not support GM’s contention that GM and Ford pickup trucks have comparable side-impact fire performance and that differences in driver demographics and driver behavior explain the difference in the rates of fire-related and MHE=fire fatalities in side-impact crashes for the GM and Ford pickups. This is demonstrated by the tremendous reduction in the rate of MHE=fire side-impact fatalities that occurred after GM moved the fuel tanks for these pickups inside the frame rails in model year 1988.

6. Contrary to GM’s contentions, the MHE coding in FARS is a reliable indicator of the number of fatalities actually caused by fire.

7. FARS data indicate that, if past trends continue, there would be approximately five additional fatalities due to fire in side-impact crashes in 1994 compared to what would occur if the subject vehicles had the same side-impact fire performance as Ford full-sized pickups.

8. Reports of non-fatal burn injuries indicate that, if past trends continue, there would be three to four additional non-fatal burn injuries in 1994 in side-impact crashes involving the subject vehicles compared to the Ford pickups.

9. Laboratory crash data indicate that, at certain impact speeds and configurations, the subject vehicles will leak fuel in side impacts, while comparable Ford pickups will not.

10. While the crash severities in fatal side-impact, fire-involved crashes involving the subject vehicles are far in excess of the severity specified in FMVSS No. 301, they are generally less than the severities that result in fires in fatal side-impact crashes involving the Ford pickups.

11. GM was aware at the time it designed the subject vehicles in the early 1970s that side-mounted fuel tank design presented an increased risk of post-crash fuel fed fires in side impacts, compared to the risk associated with other feasible alternative designs. Moreover, GM obtained additional information demonstrating the increased risk associated with the side-mounted tanks during the 15-year period the subject vehicles were in production.
R. CONCLUSIONS

1. The increased risk of death and injury from fire in side-impact crashes involving the subject vehicles is a result of the design of their fuel storage system, primarily the location of the fuel tanks outside of the frame rails, supplemented by other features of the design.

2. Given the state of the art at the time and GM’s awareness of the likely consequences, it was unreasonable for GM to design the subject vehicles with fuel tanks outside the frame rails.

3. The increased safety risk due to post-crash fires in the subject vehicles is unreasonable.

Therefore, on the basis of the entire investigative record, I have initially decided, pursuant to 49 U.S.C. § 30118(a) (formerly section 152(a) of the National Traffic and Motor Vehicle Safety Act), that the subject vehicles contain a defect that relates to motor vehicle safety.

Federico Peña